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DOI:

[10.1080/10255842.2013.771179](https://doi.org/10.1080/10255842.2013.771179)

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Document Version

Peer reviewed version

Citation for published version (Harvard):

Bahraseman, HG, Hassani, K, Navidbakhsh, M, Espino, DM, Sani, ZA & Fatourae, N 2014, 'Effect of exercise on blood flow through the aortic valve: a combined clinical and numerical study', *Computer Methods in Biomechanics and Biomedical Engineering*, vol. 17, no. 16, pp. 1821-1834.

<https://doi.org/10.1080/10255842.2013.771179>

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Eligibility checked August 2015

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Effect of exercise on blood flow through the aortic valve: a combined clinical and numerical study

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Abstract: The aim of this study was to measure the cardiac output and stroke volume for a healthy subject by coupling an echo-Doppler method with a fluid-structure interaction simulation at rest and during exercise. Blood flow through aortic valve was measured by Doppler flow echocardiography. Aortic valve geometry was calculated by echocardiographic imaging. A Fluid-Structure Interaction simulation was performed, using an Arbitrary Lagrangian-Eulerian mesh. Boundary conditions were defined by pressure loads on ventricular and aortic sides. Pressure loads applied brachial pressures with (stage 1) and without (stage 2) differences between brachial, central and left ventricular pressures. FSI results for Cardiac output were 15.4% lower than Doppler results, for stage 1 ($r = 0.999$). This difference increased to 22.3% for stage 2. FSI results for stroke volume were undervalued by 15.3% as compared to Doppler results at stage 1 and 26.2% at stage 2 ($r = 0.94$). The predicted mean backflow of stroke blood was 4.6%. Our results show that numerical methods can be combined with clinical measurements to provide good estimates of patient specific cardiac output and stroke volume at different heart rates.

Keywords: cardiac output; echo-Doppler flow; fluid-structure interaction; stroke volume.

1. Introduction

Despite progress in prevention, diagnosis, and treatment of cardiac disease, this is still the main cause of death in industrialized nations (*Murphy & Xu, 2012*). Measurement of cardiac output is a key factor in detecting the development of cardiovascular diseases and making relevant clinical decisions (*Criner et al., 2010*). For example, heart failure could be explained as failure of the heart to maintain a cardiac output that supplies the metabolic demands of the body (*Smith & Yeung, 2010*). Therefore, monitoring of cardiac function during blood pumping and measuring of stroke volume, are important for diagnosis of such diseases. Currently, invasive methods are typically used to measure cardiac output and/or stroke volume. However, such procedures are difficult, expensive, and can have risks associated with them (*Lavdaniti, 2008*). Computational methods, however, have the potential to determine cardiac output and stroke volume removing the need for invasive procedures.

Several clinical methods exist for measuring cardiac output including angiography, catheterization, MRI, and ultrasound. Some of these methods are invasive, while others require the availability of large scale and expensive equipment (*Hofer et al., 2007; Engoren & Barbee, 2005; Lavdaniti, 2008*). Clinically, it has been shown that cardiac output and stroke volume can be determined from the consumed breath-by-breath oxygen and released carbon monoxide, during exercise on a bicycle (*Knobloch et al., 2007a*). That study used non invasive ultrasound-Doppler imaging on healthy adult athletes. The measurements were taken from a rest position and continued by increasing the patient's velocity on a bicycle. They found correlations between cardiac output, cardiac index, heart rate, stroke volume and consumed O₂. *Sugawara et al. (2003)* tried to calculate cardiac output using a model-flow method. They compared their results to the data extracted by echo-Doppler and claimed the model-flow technique gave more accurate cardiac output measurements than echo-Doppler. *Knobloch et al. (2007b)* compared two clinical techniques, USCOM (ultrasound cardiac

output monitoring) and STRINGER (Stringer's formula for non-invasive hemodynamics in exercise testing; *Stringer et al. 1997*), which were used to measure cardiac output. While in a study by Christie *et al.*, (1987) three different methods were used to estimate and compare cardiac output. Maroni *et al.*, (1998) instead used a first-pass radionuclide ventriculographic method to calculate cardiac output and even diagnosed myocardial dysfunction. However, a non-invasive and inexpensive but relatively harmless method to determine cardiac output is currently not available.

Computational methods have the potential to predict cardiac output, provided the correct boundary conditions are applied. In particular, simultaneous Fluid-Structure Interaction (FSI) simulations are well suited to heart valve modelling. This is because opening and closure of the aortic valve is caused by the flow of blood (Caro *et al.*, 1978) and altered by flow patterns (Bellhouse, 1972). Iterative approaches can be used but instabilities may arise (Peskin, 1972 & 1977). As the deformation of the valve alters the flow patterns, a simultaneous approach is ideal. FSI simulations determine the reaction force that a fluid exerts on the structure with which it shares a boundary (Dowell & Hall, 2001; Wall *et al.*, 2006; Van de Vosse *et al.*, 2003). The fluid velocity is constrained to be equivalent to the structural time-dependent deformation, this ensures a two-way, and simultaneous, coupling (Dowell & Hall, 2001; Wall *et al.*, 2006; Van de Vosse *et al.*, 2003). This method requires the use of an Arbitrary-Lagrange-Euler (ALE) mesh to analyse both structural deformation (by Finite Element Analysis, FEA) and Computational Fluid Dynamics, CFD (Donea *et al.*, 1982; Formaggia & Nobile, 1999).

Recently, FSI has been used to investigate biological (Al-Atabi *et al.*, 2010; Espino *et al.*, 2012a & 2012b) and mechanical (Stijnen *et al.*, 2004; Xia *et al.*, 2005) heart valves. The aortic valve, for example, has been simulated in two- (De Hart *et al.*, 2000) and three-dimensions (De Hart *et al.*, 2003a), and its leaflets have been simulated as fiber reinforced

composites (De Hart *et al.*, 2003b). Such models demonstrate the feasibility to develop complicated aortic valve models. However, so far they have not been combined with non-invasive clinical measurements to predict a patient's cardiac output. Changes to such predictions due to heart rate (e.g. due to exercise) have not been analysed either. Heart rate is an important parameter to consider because it can cause large differences in cardiac output.

The aim of this study, therefore, was to calculate cardiac output and stroke volume during exercise using a two-dimensional FSI model of the aortic valve. The boundary conditions applied were based on the calculation of brachial pressures and accounted for differences in brachial, central and left ventricular pressures. The model operated as a natural aortic valve: an increasing systolic pressure caused valve opening and blood flow was ejected through the aortic artery. At the end of systole, as ventricular systolic pressure decreased, the aortic valve came to closure. Therefore by combining non-invasive pressure measurements with an FSI simulation it was possible to calculate: peak velocity, mean velocity, velocity-time integration, cardiac output, and stroke volume. These predictions were specific to the volunteer because the two-dimensional model geometry and boundary conditions were determined from measurements on the volunteer. In a clinical setting material properties would not be available, therefore, these were taken from the literature. Model validation was performed by comparing results to measurements from echocardiography (ECG).

2. Methods

2.1 Design of experiment

A healthy male, aged 33, participated in this study with his haemodynamic data recorded during rest and exercise. Such data has been compared to FSI simulation results. Informed consent was obtained for the participant according to protocols approved by the Department of Cardiovascular Imaging (Shaheed Rajaei Cardiovascular, Medical and Research Center, Tehran, Iran). Following physical examination, the volunteer was found to have normal cardiovascular performance, as determined from maximal bicycle exercise tests, and Doppler ECG.

Exercise consisted of the volunteer pedaling on a bicycle, with the required images of blood flow through the aortic valve obtained from the heart's five chambers view in apex region by B-mode. The brachial pressure was recorded from subject's left arm. Exercise regimes consisted of the subject raising his heart rate to approximately, around 180 beats per minute (bpm) by maximal bicycle exercise tests.

Section 2.2 describes the cardiovascular measurements and their use to calculate relevant haemodynamic parameters used to define the geometry and boundary conditions of the model. The FSI model simulated is described in section 2.3. Note the FSI model has, therefore, been used to determine flow through the aortic valve at a range of heart rates.

2.2 Cardiovascular measurements

Echocardiography

A commercially available ultrasonograph (Maylab, 60, BIOSOUND ESAOTE Inc., USA) was used for ECG examinations. A 4 MHz phased-array probe was located at the position of the heart's five chambers view at the apex region in order to record blood flow through aortic valve. The aortic valve geometry was obtained by placing a transducer at the position of the heart's three chambers view. Blood flow was estimated by echocardiogram Doppler (echo-

Doppler) flow at different heart rate stages from rest to maximal bicycle exercise test. The subject fixed his back to the bicycle chair to aid high quality images by ECG. Echo-Doppler images were stored digitally and analysed at a later stage using Maylab-desk analyzer (Maylab, BIOSOUND ESAOTE Inc., USA). Only high-quality images were accepted for subsequent use.

Peak ventricular systolic pressure and minimum central diastolic aortic pressure

Systolic and diastolic pressures of the brachial artery were measured and related to heart rate changes at rest and exercise (Figure 1). Equations 1 and 2 were used to determine the central pressure from brachial pressure measurements. This relationship was previously determined by comparing brachial pressure (acquired by Oscillometry) to the central pressure acquired using an invasive method (Park *et al.*, 2011).

$$\text{Central systolic pressure} \approx \text{Brachial systolic pressure} + 2.25 \quad 1$$

$$\text{Central diastolic pressure} \approx \text{Brachial diastolic pressure} - 5.45 \quad 2$$

where all pressures were measured in *mmHg*.

We intended to calculate left ventricular systolic pressure and central systolic pressure. Previously, a pressure difference of around 5 mmHg was found between peak left ventricular systolic pressure and central systolic pressure, using catheterization (Laske *et al.*, 1996). The ventricular, brachial, and central pressures measured are presented in Figure 1.

Ejection time

The ejection time was derived from Doppler-flow imaging under B-mode. Maylab-desk software was used to calculate the ejection time with respect to the Doppler-imaging baseline and the related ECG, simultaneously. This was done by tracing the Doppler flow with a more regular border and a larger area. Note, the ejection time is an important factor for plotting left

ventricular systolic pressure.

Time dependent left ventricular pressure

Figure 2 shows the general waveform of left ventricle pressure versus ejection time (Guyton & Hall, 1996). This waveform enabled us to derive left ventricular pressure waveform versus ejection time for each heart rate, including ejection time, left ventricular systolic pressure peak and central diastolic pressure. To do this, a scanned plot of the left ventricular pressure waveform versus ejection time was analysed using GetData Graph Digitizer (v 2.22). This software obtains original (Pressure, time) data from the scanned plot and provides values for maximum/minimum ejection time and maximum pressure at the systolic pressure peak. The minimum central diastolic pressure at the start of diastole was also determined this way (figure 2). These measurements provided the inflow boundary condition for the FSI model (*section 2.3, boundary conditions*).

2.3 Fluid-Structure Interaction simulation

Geometry

The intention was to measure cardiac output at the cross-section of the aortic valve annulus. Therefore, aortic valve geometry was obtained with respect to T-wave of ECG (maximum opening area). Diameters of the aortic valve annulus and the sinus valsalva were measured at the peak T-wave time using a resting para-sternal long-axis view. All required geometrical data is provided in Table 1. Using this data, a two-dimensional model of the aortic root and chamber of aortic sinus valsalva was created (Figure3) using Solidworks (Solidworks v2011, Dassault Systèmes SolidWorks Corp, France). The thickness of heart valve leaflets are not uniform (Clark & Finke, 1974). In our model, however, we assumed the leaflets to have a uniform thickness (0.6 mm).

Material properties

The two leaflets were considered to be isotropic, homogenous and to have a linear stress-strain relationship. Blood was assumed to be an incompressible and Newtonian fluid. This is a valid assumption under large scale flow, as occurs through the left ventricle out towards the aorta (Caro *et al.*, 1978). All material properties are provided in table 2 and were obtained from the literature (Govindarajan *et al.*, 2010; Koch *et al.*, 2010).

Boundary conditions

For *fluid boundaries* (figure 1), pressure was applied at the inflow boundary of the aortic root at left ventricular side. The applied left ventricular pressures, for different heart rates, are shown in figure 4. Note, the peak pressure increased with heart rate but the peak time of each curve decreased with increasing heart rate.

The condition of central diastolic pressure, which was heart rate dependent (figure 1), was applied at the outflow boundary of the aortic heart valve (figure 3). The walls of the aorta were set as no-slip and rigid boundaries (i.e. 0 m/s for the non-moving aortic walls). The flow condition at the shared boundaries of the valve leaflets in contact with the fluid domain were set to have a velocity equivalent to the velocity of the moving structure; i.e. the valve leaflet, according to equation 3.

$$u = \frac{\partial x}{\partial t} \quad , \quad v = \frac{\partial y}{\partial t} \quad 3$$

where u and v , refer to X - and Y -axis velocities, respectively, and $\partial x / \partial t$ and $\partial y / \partial t$ refer to the time-dependent displacement along the X - and Y -axes, respectively. Note, the Y - and X -axis define two orthogonal axes of a Cartesian coordinate system, where the former is parallel to inflow and outflow boundaries of the aorta and the latter is perpendicular to these (figure 3).

For *structural boundaries*, leaflets were restricted from moving at their aortic wall attachment (figure 3). Forces were induced by fluid dynamics but a virtual spring constraint was applied to limit deflection (see *Virtual spring constraint* section, below). The force on the leaflet boundaries was induced by fluid flow and led to valve deflection (see *Fluid-Structure Interaction* section below).

Virtual spring constraints

The natural aortic valve has bowl-shaped leaflets which prevent the valve from opening evenly under high pressure during exercise (Stouffer, 2008). We have used a virtual spring with the equation:

$$f_s = -K \cdot (d - d_0) \quad 4$$

to prevent excessive opening in our two-dimensional model (Comsol, 2011). Where f_s is a force/unit area, d is the displacement and K is a diagonal stiffness matrix that was given a high value (approximately 10^9) to prevent excessive opening due to pressure load at whole of simulation. d_0 is an optional pre-deformation, assigned a value of zero because spring foundations act and connect to leaflets at the maximum of Leaflets tip distance and at this time pre-deformation equals zero for linked springs. Leaflets tip distance was estimated at full opening of the aortic valve by Echo-Doppler imaging at rest. It was equal to 15.23 mm and held constant for all modeling stages at different heart rates.

Fluid-Structure Interaction

Simultaneous fluid and structure solution, and their interaction, requires constraints that enforce such coupling. A velocity constraint (equation 3) coupled fluid flow to structural deformation. Equal and opposite reaction forces produced by the fluid applied loads to the structure. This ensured a two-way coupling (i.e. simultaneous interaction). The fluid forces

are equivalent to Lagrange multipliers determined using a (non-ideal) weak formulation of fluid dynamics. This leads to the loading conditions expressed by equation 5. Fluid dynamics were solved using the continuity and incompressible Navier-Stokes equations, assuming Newtonian and laminar flow, using a full stress tensor. Further detail on these techniques is provided elsewhere (Espino *et al.*, 2012b).

$$(\boldsymbol{\sigma} \cdot \mathbf{n})_{Fluid} = (\boldsymbol{\sigma} \cdot \mathbf{n})_{Solid} \quad 5$$

where $\boldsymbol{\sigma}$ is the stress tensor and \mathbf{n} is the normal vector to the FSI boundary (Comsol, 2011). A moving ALE mesh was used which enabled a Lagrangian framework for the solid domain and an Eulerian framework for the fluid domain. The moving mesh enabled the deformation of the fluid mesh to be tracked. All other boundaries had a fixed mesh. No re-meshing was used but Winslow smoothing was applied to improve the resultant mesh (Winslow, 1966). The deformation of this mesh relative to the initial shape of the domain was also computed using hyper-elastic smoothing. Two-dimensional triangular planar strain elements were used to define the mesh. Mesh convergence was assessed in terms of stroke volume and cardiac output predictions (table 3). Predictions were stable with 7001 elements (figures 5 and 6). The number of elements was increased using predefined mesh sizes which ranged from extremely-coarse (1400 elements) to extra-fine (19865 elements) for our model. FSI simulations modelled two difference scenarios (termed stages). A stage with (stage 1) and without (stage 2) the valvular-arterial pressure differences between the aortic root at the left ventricle and the brachial artery were modelled. Results from these two stages demonstrate the effect of pressure-drops in the predicted results (see section 3.1).

Analysis

The finite element analysis package Comsol Multi-physics (v4.2) was used to solve the FSI model under time dependent conditions. The structural mechanics package was used to

analyse the leaflets. This enabled the use of a large deformation setting allowing determination of Green strains and Cauchy stresses, as reported previously (Espino *et al.*, 2012c).

A direct MUMPS (MULTifrontal Massively Parallel sparse direct Solver; Comsol, 2011) solver was used for the time-dependent simulation. Transition from one time step to the next occurred once the estimated model error was below a set tolerance. A Newtonian iteration was used, as discussed previously (Espino *et al.*, 2012c).

Calculation of cardiac output & validation

Cardiac output was computed using equation 6:

$$\text{Cardiac output} = \text{Stroke volume} * \text{Heart rate} \quad 6$$

where the stroke volume was calculated from ECG using equation 7:

$$\text{Stroke volume} = \text{Velocity integration} * \text{Aortic area} \quad 7$$

where the velocity integration was automatically obtained by tracing the Doppler flow from ultrasound imaging. The aortic area was calculated using equation 8:

$$\text{Area} = \pi \left(\frac{D}{2} \right)^2 \quad 8$$

where D is the measured ascending aortic diameter after the sinotubular junction (table 1).

For FSI simulations, the mean velocity numerically was obtained at each time step of the ejection period as shown in figures 6(a) and 6(b). Equation 9, however, was used to determine the velocity integration (used to determine both stroke volume and cardiac output).

$$\text{Velocity intergration} = \int_0^{\text{Ejection time}} V . dt \quad 9$$

where V is the fluid-velocity through the outlet boundary. Stroke volume and cardiac output predicted from FSI simulations were compared to values determined by echo-Doppler. Note that the mean velocity for each heart rate was obtained using equation 10.

$$\textit{Velocity mean} = \frac{\textit{Velocity integration}}{\textit{Ejection time}}$$

10

Comparison of measurements of mean velocity, cardiac output and stroke volume enabled quantitative validation of the FSI model.

3. Results

3.1 Comparison of numerical and clinical haemodynamic predictions

The velocity-ejection time graphs are shown in Figures 6(a) and 6(b) for different heart rates at rest and during exercise. Tables 4 and 5 presents the data predicted from FSI simulations and echo-Doppler. The peak blood flow velocity through aorta increased by 16.6% from 98 bpm to 147 bpm, and increased a further 2.3% as the heart rate increased to 169 bpm. Figure 6(b) shows results that exclude differences between the brachial, central and aortic root pressure at left ventricle for the velocity profiles obtained from FSI simulations at rest and for the time of exercise. When only the brachial pressure was applied as the boundary condition, velocity profiles had fewer velocity peaks than when pressure differences were accounted for. When pressure differences were accounted for, model predictions were more reliable.

The mean velocity predicted by FSI simulations was on average 14.8% lower than Echo Doppler measurements (i.e. an average for the whole protocol) when pressure differences were accounted for. This difference increased to 22.4% when the pressure differences were not accounted for (Table 4). Cardiac output predicted by FSI simulation was on average 15.4% lower when compared to Echo-Doppler results, for the whole of protocol, when pressure differences were accounted for. The corresponding difference, when pressure differences were excluded, was 22.3%.

FSI simulations, that accounted for pressure differences, predicted a stroke volume that was on average 15.3% lower than that derived from Echo-Doppler. This increased to 26.2% when pressure differences were ignored.

For FSI simulations, the mean velocity increased by 15.7% as the heart rate increased from 98 bpm to 136 bpm when pressure differences were accounted for and increased by 4.6% from a heart rate of 136 bpm to 169 bpm. When pressure differences were accounted for, FSI simulations showed a 2.9% increase in stroke volume from a heart rate of 98 bpm to 114

bpm. Then this approximately stopped from heart rates of 136 bpm to 147 bpm. In addition there is a 5% decrease in stroke volume from heart rate of 147 bpm to 169 bpm (figure 7a). The cardiac output (including pressure differences) increased by 60.2% from a heart rate of 98 bpm to 169 bpm (figure 7b). This led to an increment in cardiac output of 5984 ml/min. There were less differences between Doppler-derived data and numerical stage 1's results (i.e. accounting for pressure differences) than stage 2 results for cardiac output and stroke volume. Consequently, FSI simulation that included pressure differences were chosen to continue this study. These results also demonstrate the importance of including the valvular-vascular pressure-drops in our study.

3.2 Correlation between FSI and Echo-Doppler results

Regression analysis between echo-Doppler and FSI simulations led to a correlation gradient of 0.802 (figure 8a) for cardiac output and 0.764 (figure 8b) for stroke volume. The *y-axis* intercepts for these correlations were 669.1 ml/min and 15.05 ml/beat for cardiac output and stroke volume, respectively. There was a high correlation between estimations from echo-Doppler and FSI simulations for cardiac output ($r = 0.999$) and stroke volume ($r = 0.940$). Therefore, there was a strong correlation between the two methods and similar values were predicted.

3.3 Numerical prediction of blood backflow while accounting for pressure differences

Table 6 provides the backflow values during valve closure, when the pressure difference between brachial and central/left ventricle was considered. At 98 bpm total cardiac output was computed to be 9884 ml/min. Backflow averaged 489 ml/min. This led to the estimation of 4.6% backflow at the closure phase, on average.

The FSI simulations predicted an increase in backflow with increased heart rate, this

increased per minute by 74% from a heart rate of 98 bpm to 169 bpm. The backflow increased to 498 ml/min, and total blood volume ejected from left ventricle was 10373 ml/min. Moreover, backflow velocity peak increased 43% as heart rate increased from 98 bpm to 169 bpm (table 6).

3.4 Comparison of numerical and clinical correlation between cardiac output and brachial pressure

The relationship between cardiac output and the brachial systolic and diastolic pressure difference is shown in Figure 9. A good correlation was determined using a quadratic polynomial equation, for both echo-Doppler and FSI simulations. However, a pressure difference can be estimated between the FSI simulation and the echo-Doppler derived curve. For instance, echo-Doppler derived cardiac output for the pressure difference of 70 mmHg resulted in 11356 ml/min. The FSI simulation, instead, estimated a cardiac output of 11356 ml/min at 87 mmHg. This 17 mmHg difference could be due to a valvular and arterial pressure drop. An increase in the brachial pressure difference reduces this pressure drop (Figure 9).

4. Discussion

4.1 Study findings

The study has combined haemodynamic measurements with an FSI model to non-invasively calculate the cardiac output and stroke volume from a healthy subject during exercise. Echo-Doppler derived data has been compared to FSI predictions. To our knowledge this is the first time that an FSI model has been combined with exercise measurements to enable numerical predictions of cardiovascular performance. When valvular-vascular pressure differences were accounted for (stage 1), the predicted cardiac output (using FSI) was lower on average by 2415 ml/min than Doppler-derived, as opposed to 3502 ml/min when such pressure was not accounted for (stage 2). Improved precision of the measured valvular and arterial pressure differences could further reduce the difference between the two methods. Despite the use of a simplified two-dimensional model, FSI predicted values were to within 84.6% of the values of Doppler-measured. The FSI model reliably predicted cardiac output and mean aortic velocity over a range of heart rates. Predictions of around 85% of experimental measurement would present limitations in clinical use, therefore, linear correlations have been used. This enables predictions derived from the FSI model to be obtained which are highly accurate (e.g. $r = 0.94$ and 0.999 for stroke volume and cardiac output, respectively). This study demonstrates the feasibility of obtaining a range of time-dependent and variable boundary conditions (e.g. altered due to exercise) and generate a simplified two-dimensional model that can predict cardiovascular performance within relatively short solution time (<20 minutes).

4.2 Clinical application & reliability

Catheterization-Thermodilution is the golden standard for measuring cardiac output (Lavdaniti, 2008). However, it is an invasive method with potential risks such as heart failure, cardiac arrhythmia, and even death (Lavdaniti, 2008). Additionally, Thermodilution exposes

the patient and physician to harmful radiation. Exercising while catheterized also causes a range of technical problems and, thus, is not common practice. However, the use of a numerical method allows the prediction of cardiac function by non-invasive measurements throughout an exercise protocol.

Numerical simulation allows easier and more precise estimation of cardiac output than using echo-Doppler. Also, it does not have inter- and intra-observer validity variables that are the case for executing ECG. Such variability depends on personal proficiency and the image capture capability of the user. Therefore, the key-concern is the reliability of numerical methods when predicting cardiac output.

Our FSI model led to a good cardiac output correlation with Doppler-derived values ($r = 0.999$), in addition a good correlation ($r = 0.94$) was achieved for stroke volume. Data gained when accounting for pressure differences between brachial and central to aortic root at left ventricle, led to differences of 17.9 ml/beat for stroke volume on average. This increased to 26.2 ml/beat when such pressure differences were ignored. There was also a good correlation with the mean velocity ($r = 0.94$) but the correlation for predicted peak velocity was lower ($r = 0.73$). However, in the latter case, errors related to Doppler flow tracings may have lowered this correlation. For example, oscillations were observed at the echo-Doppler flow tip which may have reduced the operator's tracing precision.

4.3 Comparison to literature

Following a literature search we have not found a previous comparable study that combined a clinical and numerical approach to predict cardiac function during exercise. In our study, patient specific cardiac output was predicted at a range of heart rates induced by exercise. However, our study compares well to other numerical studies used to predict cardiac output at rest. Our model predicted a cardiac output at rest of 9017 ml/min, comparable to

predictions between 3400 - 7500 ml/min (Korakianitis & Shi, 2006; Kim *et al.*, 2009). Such predictions have used a finite element method with a lumped parameter technique, a Wind-Kassel model (Korakianitis & Shi, 2006), and an electrical integration circuit (Podnar *et al.*, 2002). However, Podnar *et al.* (2002) predicted no increase in cardiac output with increased heart rate (5500 ml/min at 120 bpm, but 5300 ml/min at 150 bpm). This is in disagreement with our results, as we found cardiac output to increase with heart rate. Data derived from Christie *et al.* (1987) agrees with our results. Therefore, it is likely that the lack of validation with clinical data, by Podnar *et al.* (2002), led to some inaccuracies at increased heart rates. Moreover, it should be noted that a non-athlete, can be expected to have a maximum stroke volume of 110 ml with a heart rate of 195 bpm (Guyton & Hall, 1996; Porth & Glenn 2010). Since our subject is a non-athlete, our numerical results are in good agreement with the literature.

4.4 Limitations & future trends

This model has been used to make patient specific predictions for cardiac output, in combination with non-invasive brachial pressure measurements. A notable simplification used for our FSI model was the use of a constant orifice area and a single diameter for the ascending aorta. The regression analysis between predicted and measured cardiac output and stroke volume enable true values to be calculated from predicted model values (using the equations provided in figure 8). Therefore, even though the model may predict a value that is approximately 15% in 'error', the true clinical value can still be derived using our existing simplified model. Validation showed good agreement with a range of haemodynamic parameters although with differences between experimental and numerical predictions. For clinical applications further accuracy may be necessary which may be improved by addressing key limitations.

One limitation is that the model was solved in two-dimensions, the predictions might improve by use of a three-dimensional model. The feasibility of developing such models is well established (De Hart *et al.*, 2003a & 2003b). However, a two-dimensional model has the advantage of a shorter solution time and this assumption has been made before for 2D valves (e.g. De Hart *et al.* 2000). Our model solved within 15 minutes which, clinically, would be a reasonable waiting time. It should be noted that existing clinical equipment have large associated errors. For example, the commercially available ultrasonograph (Maylab, 60, BIOSOUND ESAOTE Inc., USA), which was used for our study and is used clinically, has a reported accuracy of $\pm 11\%$ for the stroke volume and subsequently for the cardiac output (Maylab advanced operation, 2008).

Another limitation is that the mechanical properties of the valve leaflets specific to the volunteer are unknown. There is a large variation in the mechanical properties of all heart valves (Clark *et al.*, 1973) and their components (Millard *et al.*, 2011). Although we have used accepted values in the literature, mechanical properties for each subject are not measurable. We applied a $\pm 30\%$ change in Young's modulus (table 7) and found that the predicted cardiac output varied by no more than 5% . It is notable that, Kortsmit (2009) reported such variation in Young's modulus for native aortic heart valve.

The assumption of rigid aortic walls was a model limitation but enabled a faster simulation time (important clinically). This limitation may contribute to the model predictions being lower than the real values measured. However, the main aim of the study was to look at the aortic valve. Consideration of the aortic wall may enable a better model in future studies. The model was also assumed isotropic, homogenous and linear. This may have contributed to our values under-predicting cardiac output and stroke volume. This assumption, though, is consistent with previous studies that have led to reasonable approximations of valve function (De Hart *et al.*, 2000 & Espino *et al.*, 2012a & 2012b).

Finally, a plane-strain simulation ignores out of plane effects assuming the model to be a standard cross-section of the valve. This assumption might affect cardiac output and stroke volume predictions. However, we used an equation to mimic out-of plane restraint to reduce some of these errors. Additionally models which are not intended for use in three-dimensional stress states include only plane strain terms (Weinberg & Kaazempur-Mofrad, 2005). Despite these above errors the trends were predicted quite well by the model, despite a 10-15% difference in magnitude. Moreover, the Simplified 2D model has the advantage of solving in 6 to 15 minutes (with the computers assembled: 8Gb Ram, Core i5, 2.2 GHz) over different heart rates, which may be important clinically. Regardless of model errors, there was a very strong correlation between predicted and measured cardiac output ($r = 0.999$) and stroke volume ($r = 0.94$). Therefore, it is feasible to correct for predicted values (using the derived equations in figure 8). Such methods are well established when combining a model with experimental measurement (Christie et al., 1987; Maroni et al., 1998, Sugawara et al. 2003, Park et al., 2011).

Clinical assessment of cardiac function is gathered on the basis of statistical information and generalization. This might be considered as another limitation of our model as one subject was investigated. However, a numerical simulation needs specific values such as boundary conditions, mechanical properties, and geometric dimensions. A range of values, for statistical comparison, cannot be predicted unless stochastic modelling is applied to account for variability (Espino *et al.*, 2003). Instead, subject specific predictions from our FSI model were validated against directly comparable measurements. This has enabled quantitative assessment of the reliability of our model. Currently, there is a trend towards patient specific models in medical research (e.g. Öhman *et al.*, 2011). This is due to the potential benefits in using numerical methods to aid treatment/diagnosis for individual patients. Recently, for example, such a three-dimensional model was generated for an ischemic mitral valve (Wenk

et al., 2010). This presents possible applications for our combined numerical and clinical approach to investigate cardiac output during disease, including aortic valve stenosis or even calcification; e.g. by multi-scale modelling (Weinberg & Kaazempur-Mofrad, 2008).

5. Conclusion

We have introduced a two-dimensional fluid-structure interaction model of aortic valve which was able to reliably predict cardiac output and stroke volume. Our model predicted mean velocity, stroke volume and, cardiac output to within 14.8%, 15% and 15%, respectively, of Doppler-echocardiography measurements. Strong correlations were determined for predicted and measured cardiac output ($R = 0.999$) and stroke volume ($R = 0.94$) which enables correction of the numerical values predicted using regression equations. The advantage of using a simple two-dimensional model was the relatively quick solution time of less than 15 minutes (important within a clinical setting). The model developed was used to make predictions both during rest and exercise.

ACKNOWLEDGEMENTS

DME is currently supported by a Marie Curie Intra-European Fellowship within the 7th European Community Framework Programme (Programme number: FP7/2007-2013; under grant agreement n°252278).

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TABLES

Table 1. Geometric data of the aortic valve.

Maximum diameter of normal aortic root (mm)	Ventricular side diameter (mm)	Aortic side diameter (mm)	Ascending aorta diameter after sinotubular junction (mm)	Leaflet's length (mm)	Valve's height (mm)
33.3	22.2	23	23.5	16.6	20.36

Table 2. Mechanical properties

Viscosity (Pa.s)	Density (kg/m ³)	Young's modulus (N/m ²)	Poisson ratio
3.5×10^{-3}	1056	6.885×10^6	0.4999

Table 3. Investigation of mesh independency on predicted stroke volume and cardiac output, while considering valvular-arterial pressure differences, for heart rate of 98 bpm.

Number of elements	1400 (Extremely coarse)	1944 (Extra coarse)	2194 (Coarser)	2648 (Coarse)	3669 (Normal)	5301 (Fine)	7001 (Finer)	19865 (Extra fine)
Stroke volume (ml/beat)	94.9	95.2	96.7	96.1	99.1	100.7	100.9	100.9
Cardiac output (ml/min)	9300	9329	9476	9417	9711	9868	9888	9891
Solution time (s)	577	610	633	659	706	782	897	15807

Table 4. Comparison of Doppler-Echocardiography to Numerical modeling results

HR (bpm)	VSP /CDP (mmHg)	VSP* /CDP* (mmHg)	VPD (m/s)	VPN (m/s)	VPN* (m/s)	VMD (m/s)	VMN (m/s)	VMN* (m/s)	COD (ml/min)	CON (ml/min)	CON* (ml/min)
98	152/68	144/74	1.49	1.51	1.36	1.05	0.89	0.79	11356	9884	8773
106	158/65	152/71	1.50	1.59	1.48	1.10	0.95	0.86	12651	10864	9935
114	165/63	157/69	1.58	1.67	1.54	1.11	1.00	0.90	14051	11829	10672
125	169/63	163/69	1.60	1.70	1.59	1.21	1.03	0.94	15298	12884	11938
136	174/64	167/70	1.79	1.74	1.62	1.24	1.03	0.95	16172	13518	12489
147	178/65	171/71	1.58	1.76	1.65	1.25	1.05	0.97	17225	14600	13424
153	180/66	173/72	1.74	1.77	1.66	1.24	1.03	0.97	17330	14625	13655
159	182/67	175/72	1.77	1.78	1.68	1.26	1.06	0.97	17941	15108	13961
169	186/68	178/74	1.63	1.80	1.68	1.28	1.08	0.98	18849	15832	14504

HR: Heart rate;

VSP: Ventricular systolic pressure;

CDP: Central diastolic pressure;

CON: Cardiac output by numerical simulation;

COD: Cardiac output by Doppler;

SVN: Stroke volume by numerical simulation, per beat;

SVD: Stroke volume by Doppler, per beat;

VPD: Peak velocity by Doppler;

VPN: Peak velocity by numerical simulation;

VMD: Mean velocity by Doppler;

VMN: Mean velocity by numerical simulation.

*Calculated without considering the effects of valvular-arterial pressure differences.

Table 5. Comparison of Doppler-Echocardiography to Numerical modeling results in terms of stroke volume for both stages considering the effects of valvular-arterial pressure differences and not considering them.

Heart rate (bpm)	SVD (ml/beat)	SVN (ml/beat)	SVN* (ml/beat)	Sugawara et al, 2003. (ml/beat)	Christie et al, 1987. (ml/beat)	Percentage of difference of SVN to SVD
98	115.8	100.9	89.5	80	102.4	12.9
106	119.4	102.5	93.7	83	108	14.1
114	123.3	103.8	93.6	86	109.5	15.8
125	122.4	103.1	95.5	89	105	15.8
136	118.9	99.4	91.8	92	100.6	16.4
147	117.2	99.3	91.3	94	100.5	15.2
153	113.3	95.6	89.2	Na	102.5	15.6
159	112.8	95	87.8	Na	103.6	15.8
169	111.5	93.7	85.8	Na	104.7	16

SVN: Stroke volume by numerical simulation, per beat;

SVD: Stroke volume by Doppler, per beat;

*Calculated without considering the effects of valvular-arterial pressure differences.

Table 6. Numerical simulation estimates of back-flow during closing phase

Heart rate (bpm)	VPB (m/sec)	SVB (ml/beat)	COB (ml/min)
98	-0.70	-5.00	-489
106	-0.82	-5.32	-563
114	-0.88	-5.38	-613
125	-0.90	-5.11	-637
136	-0.95	-5.45	-740
147	-0.94	-5.28	-776
153	-1.01	-5.88	-899
159	-1.01	-5.34	-849
169	-1.00	-5.05	-853

COB: Stroke volume of backflow to left ventricular per minute;

SVB: Stroke volume of backflow to left ventricular per beat;

VPB: Backflow velocity peak.

Table 7. Change in predicted cardiac output with Young's modulus.

Young's modulus increase (%)	Change in Cardiac output (%) with heart rate								
	98 (bpm)	106 (bpm)	114 (bpm)	125 (bpm)	136 (bpm)	147 (bpm)	153 (bpm)	159 (bpm)	169 (bpm)
-30	2.2	-1.1	-0.2	-4.1	-0.5	-0.4	-3.9	-3.3	-3
-20	2.3	-2.1	-1	-3.6	-0.5	-0.1	-3.4	-2.7	-3.8
-10	-0.6	-2	-0.1	-3.1	-0.2	-0.4	2.7	-2.5	-0.8
10	-0.2	-1.1	-0.1	-1.4	0.2	-0.5	0.1	0.8	-0.3
20	-2.3	-1.4	-0.1	-2.7	0.2	-0.2	-1.7	-1.9	-0.01
30	-2.7	-0.6	0.6	-2.1	1.2	-0.2	-2.2	-2.2	-0.6

FIGURE CAPTIONS

Figure 1. Interpolated curves for brachial, central and ventricular pressures.

Figure 2. Tracings of the left ventricular systolic pressure waveform.

Figure 3. Aortic valve model. Note, dimensions are provided in table 1.

Figure 4. Pressure wave-forms of left ventricle during ejection for different heart rates.

Figure 5. Mesh for the (a) valve cusps and (b) elements on a cusp of the solid domain mesh generation. (c) the fluid domain mesh generation.

Figure 6. FSI's predictions of (a) velocity spectrums which consider a valvular-arterial pressure difference effects (Stage 1). FSI's predictions of (b) velocity spectrums without valvular-arterial pressure differences effects (Stage 2). Note, HR refers to heart rate and ET to ejection time.

Figure 7. Comparison of (a) stroke volume and (b) cardiac output when valvular-arterial pressure differences were (Broken line) and were not included (Dotted line), and the Doppler-derived measurement (Solid line).

Figure 8. Regression plot (a) comparing Doppler-derived cardiac output (COD) and numerical simulation (CON). (b) Regression plot comparing Doppler-derived stroke volume (SVD) and numerical simulation (SVN).

Figure 9. Regression plot (Solid lines) comparing cardiac output data given by Echo-Doppler (triangular points) vs. Numerical method (squared point) related to brachial systolic and diastolic pressure difference. Note, CON: Cardiac output by numerical simulation; COD: Cardiac output by Doppler; BPD: Brachial pressure difference.