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Perceived Intensities of Normal and Shear Skin Stimuli using a Wearable Haptic Bracelet

Mine Sarac^{1,4}, Tae Myung Huh², Hojung Choi¹, Mark R. Cutkosky¹, Massimiliano Di Luca³, and Allison M. Okamura¹

Abstract-Our aim is to provide effective interaction with virtual objects, despite the lack of co-location of virtual and real-world contacts, while taking advantage of relatively large skin area and ease of mounting on the forearm. We performed two human subject studies to determine the effects of haptic feedback in the normal and shear directions during virtual manipulation. In the first study, participants performed significantly better while discriminating stiffness values of virtual objects when the feedback consisted of normal displacements compared to shear displacements. Participants also commented that they could detect normal cues much easier than shear, which motivated us to perform a second study to find the point of subjective equality (PSE) between normal and shear stimuli. Our results show that shear stimuli require a larger actuator displacement but less force than normal stimuli to achieve perceptual equality for our haptic bracelets. We found that normal and shear stimuli cannot be equalized through skin displacement nor the interaction forces across all users. Rather, a calibration method is needed to find the point of equality for each user where normal and shear stimuli create the same intensity on the user's skin.

I. INTRODUCTION

In the real world, mechanical properties of objects, such as mass, stiffness, and temperature, can be perceived via touch (Fig. 1(a)). Haptic devices aim to recreate the same feeling for virtual interactions. Many multi-degree-of-freedom fingertip devices have been developed to render the interaction forces during active exploration/manipulation tasks in a virtual environment, as shown in Fig. 1(b) [1], [2]. The combination of the shear and normal skin stimulation provided by these devices and the high density of mechanoreceptors in the fingerpad result in strong performance and perceived realism of manipulation tasks in virtual environments [3].

However, fingertip devices must be miniaturized to reduce encumbrance. Such a requirement complicates the design and increases the cost of actuators, which must have relatively large output force, small size and light weight. Furthermore, there are certain applications where fingertips should be left free to interact with physical objects, as during augmented reality. In these situations, users cannot wear fingertip devices which would interfere with these physical objects.

Building on previous studies that showed the significant impact of visual cues on the overall perception when ac-

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Fig. 1. Grasping tasks with different types of haptic feedback: (a) In the real world, the fingers directly contact the object. (b) In a virtual environment with fingertip haptic devices, grasp forces (F_g) are displayed on the fingertips. (c) In a virtual environment with a wearable haptic device, grasp forces are displayed on the forearm near the wrist.

companied with haptic feedback [4]–[6], we examine a different approach to artificial haptic feedback by relocating the delivery of haptic sensation from the fingertip to the arm or the wrist. In doing so, the mechanical properties of manipulated virtual objects are rendered on the arm (Fig. 1(c)). In this context, haptic feedback is computed through fingertip contact and material properties of objects is rendered on the user's arm. We propose that haptic stimulation at the wrist that represents the real properties of an object, even if not rendering them perfectly, might be sufficient to create interpretable or "believable" interactions. Such relocation could qualitatively add to (rather than detract from) the user experience without increasing cognitive or attentional load in the user.

Werarable bracelets and arm bands have been used to emulate the sensation of human touch in social interactions [7]–[9], map haptic cues to navigational directions [10] or communication [11]–[13], render interaction forces during teleoperation tasks [14] or prosthesis control [15]–[17], and improve the learning process for surgical trainees in robotic surgical systems [18]. Tasbi [19], Bellowband [20], and WRAP [21] squeeze the wrist in a distributed manner using various actuation methods to offer effective haptic solutions.

Although wrist-worn devices have been shown to improve user performance during virtual manipulation tasks, there remain questions regarding the efficacy of different degrees of freedom of haptic feedback, namely in the normal (squeeze) and shear directions. Moriyama et al. [22] developed a fivebar linkage mechanism with two degrees of freedom to present haptic feedback to the forearm during virtual interactions. They asked users to evaluate and compare different feedback directions based on the "strangeness" feeling they create on users. Their results show that normal feedback feel

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less strange than shear when applied on the wrist. Despite their inspirational ideas regarding wearable wrist devices and perception, we found it difficult to map the strangeness metric toward practical design guidelines.

The effects of force direction on users' perception, task performance, and learning curve of virtual manipulation tasks for wrist-worn devices is still unknown. Previously, we performed a set of experiments based on haptic sketches by simulating interaction forces on user's arm manually [23]. We applied normal forces and shear forces to user's wrist at the dorsal side as users interact with the virtual environment. Users reported that both normal and shear forces felt natural and intuitive with their interactions.

In this paper, we first present the results of a study that compares the user performance and perception while discriminating virtual stiffness values of objects and receiving haptic feedback in the normal and shear directions acting on the wrist. The stiffness discrimination study was previously designed and presented as an extended abstract [24]; here we fully describe the study and results. Then we investigate the difference between the perceived intensity of normal and shear stimuli in terms of actuator displacements and applied forces. Finally, we propose a perceptual model of shear displacement intensity with respect to normal.

II. HAPTIC BRACELETS

To study the effect of force direction (normal versus shear) on perception during virtual interaction, linear actuators are a promising approach because they can be implemented for both directions with identical control performance and force output. For our study, we use the Actuonix PQ12-P actuator due to a combination of size (15 g), maximum stroke (20 mm), high output force (18 N), and easy controllability via an integrated position sensor.

We selected grounding/orienting of linear actuators to enable investigation of both direction and location of forces acting around the wrist. The direction of forces is adjusted by designing different grounding parts as shown in Fig. 2. Grounding the linear actuator vertically on the wrist applies normal forces as the displacement is controlled (Fig. 2(a)). Grounding the actuator horizontally creates shear forces with



Fig. 2. Haptic bracelets worn by a user on the wrist provide skin deformation as (a) normal stimulus and (b) shear stimulus. Double-sided tape between the end-effector and the skin prevents slip during shear stimulus. The force sensor is used only for the Experiment 2.



Fig. 3. Set up for Experiment 1: A user sits in front of a monitor and wears a haptic bracelet, a fingertip sensor for the tracking system, and noise cancellation headphones. Users are asked to interact with objects in the virtual environment while the haptic device renders the interaction forces at the wrist.

double-sided tape used to prevent the end-effector from slipping on the skin (Fig. 2(b)).

III. EXPERIMENT 1: STIFFNESS DISCRIMINATION

To identify the direction in which interaction forces should be be applied to the arm to improve the perception and performance of virtual tasks, we performed a stiffness discrimination experiment using the haptic bracelets, a virtual environment, and tracking system as shown in Fig. 3.

12 subjects (age 24-31, 6 females and 6 males) participated in the study. All participants were right-handed and had previous experience with haptic interfaces. The Stanford University Institutional Review Board approved the experimental protocol and all participants gave informed consent.

A. Experiment Procedures

We created a virtual environment using the CHAI3D framework [25] as shown in Fig. 4. During the experiments, the virtual environment is displayed on a regular monitor and updated at 144 kHz. User's finger movements are tracked at approximately 200 Hz using a trakSTAR tracking system and an Ascension Model 800 sensor attached on user's finger through 3D printed grounding.

The overall experiment is composed of two parts, one for each direction of force (normal vs. shear). For each part, there is a training block with 24 trials and 3 testing blocks with 16 trials each. Each testing block renders forces from one location of forces (dorsal side / ventral side / both sides), while the training block covers all of the locations with a predefined order. Once thefirst part is completed, the participant wears the bracelet with the other force direction and repeats the entire procedure. Between each block and part, the participant was given a break time to rest as needed. Each participant performed the task in a different order.

There are two objects in the virtual environment. The stiffness value of one object is kept at 300 N/m. and the other object is pseudo-randomized among 100, 200, 400, and 500 N/m. The initial locations of these objects are randomized.



Fig. 4. Experiment 1 task: (a) Each trial has a starting zone, target zone, and two visually identical objects with different stiffness values. (b) The participant presses on each object, chooses the stiffer object based on the haptic feedback, and drags it to the purple zone. During training, the zone turns (c) red if the answer is wrong, and (d) green If the answer is correct. (e) During testing, the zone turns purple and opaque regardless the answer.

During the experiment, the participant sees two identical box objects which have different simulated stiffness values. Participants move their index finger so that their avatar in the virtual environment interacts with these virtual objects. Specifically, they press on each object, to evaluate its stiffness, and then drag the stiffer object to the target zone. The experiment has two modes: training and testing. During the training mode, the target zone changes color based on the participant's answer; if the participant's answer is correct, the zone turns green, and if the answer is wrong, the zone turns red. During the testing mode, the target zone becomes opaque to indicate completion of the task.

As the participant interacts with the virtual boxes, rendered forces are computed based on the stiffness values of the boxes. The chosen linear actuators are position controlled, so desired forces are expressed in the form of desired displacements using a fixed force-to-displacement ratio 0.03 N/mm [26]. Even though hairy skin was previously reported as having stiffness of 0.03 N/mm for normal and 0.04 N/mm for shear directions, whether skin stiffness is different for the dorsal and ventral sides of the wrist is unknown. Thus, in order to provide consistent stimuli, we kept the level of displacements (as opposed to force) the same for the different conditions for both normal and shear directions. Biggs et al. showed that hairy skin is three times more sensitive to shear displacements than normal [27], so we hypothesized that stiffness discrimination would be better when the shear bracelet is used.

B. Results and Discussion

We investigated participants' accuracy and time spent for different stiffness pairs. Fig. 5 shows that, users performed better using normal displacements than shear in general. In addition, the statistically significant differences were observed only with the comparisons of 100 N/300 N (t(11) = 2.7080, p = 0.0204) and 500 N/300 N (t(11) = 3.0225, p = 0.0116) – cases where the differences between stiffness values were the largest. There was no significant difference in time spent performing the task.

In addition to the quantitative data, we also collected subjective comments from participants about the direction of displacement they liked the most (Q1) and was easiest to notice (Q2). For Q1, 4 users chose shear and 8 chose normal, although all users stated for Q2 that normal discplacements were much easier to notice. The verbal comments of the



Fig. 5. Accuracy of participants' answers and the time spent for each trial among all locations for Experiment 1. Participants performed significantly better with normal displacements compared to shear when asked to compare objects with highly different stiffness values, but not for objects with similar stiffness values.

subjects are coherent with the analyses performed above, so we conclude that normal forces are more effective than shear for stiffness recognition in this setup.

Our results contradicted those of Biggs et al. [27] regarding sensitivity of normal versus shear force on the skin. This led us to believe that equalizing displacements using wrist-worn devices created a bias in perception because the grounding forces of the two bracelets were in different directions (parallel versus perpendicular to the direction of motion). Thus, we performed a second experiment to investigate strategies for equalization.

IV. EXPERIMENT 2: POINT OF SUBJECTIVE EQUALITY

In this experiment, we investigate and quantify differences between the perceived intensity of normal and shear stimuli on the wrist applied by a wearable haptic bracelet. Participants perceive normal and shear stimuli on separate wrists and tune the intensities until both feel the same, as shown in Figure 6. We determined the relative intensity of normal and shear stimuli based on actuator displacements, how the per-



Fig. 6. Setup for Experiment 2: A participant wears two bracelets with normal and shear stimuli. A monitor gives a visual instruction of which arm receives the reference and adjusted stimuli.

ceived intensity of normal and shear stimuli are affected by applied force, whether the point of subjective equality varies across people, and how perception of shear displacement can be modeled with respect to normal displacements.

For this experiment, the haptic bracelets are equipped with 6-degree-of-freedom (6-DoF) force sensors to measure interaction forces during the experiment and equalize the tightness of the Velcro strap on each bracelet. The custom force sensors are capacitive sensors with a design similar to [28] and were chosen for their compact form (2 cm in diameter, 3.2 mm thickness), low-cost (<\$10) and high performance compared to commercial sensors. The RMS errors between the measurements of the custom force sensor used in this experiment and a commercial ATI Gamma force sensor were 0.0752 N and 0.0617 N when calibrated in the range of < 5 N and < 6 N in the shear and normal directions, respectively. Force measurements confirm that the two bracelets generate the same amount of force but in their respective direction of actuation.

In addition to the experiment described in Section III, two prior works provided motivation for the design of this study. Diller et al. [26] performed an experiment using a grounded, flat-ended probe on the skin. Their results showed that shear forces were less than normal forces for the same actuator displacements, but how participants perceived these stimuli is not reported. As described earlier, Biggs et al. [27] compared normal and shear stimuli at the forearm in terms of perceived intensity, and found that shear displacement should be 3 times less than normal displacement in order to create a similar intensity. We hypothesize that differences in experimental setup (wearability, contact area, reference stimulus value) might change the relative actuator displacements for normal and shear stimuli, but not the interaction forces.

In this experiment, four subjects (age 25-32, 1 female and 3 males) and eight subjects (age 25-32, 3 females and 5 males) participated in the preliminary and main studies, respectively. All participants of the preliminary study also participated to the main study. All participants were righthanded and had previous experience with haptic interfaces. The Stanford University Institutional Review Board approved the experimental protocol and all participants gave informed consent.



Fig. 7. The staircase algorithm calculates the actuator displacements based on the participant's responses. The data was collected during the main study of Experiment 2 with 3 mm shear reference.

A. Experiment Procedures

Upon the participant's arrival, the experimenter spent 5 minutes adjusting the setup and explaining the experiment procedures. The participants were seated on a chair with their elbows supported by the chair and their hands supported by a desk, so that their wrists were suspended and contacted only the haptic bracelets.

The experimenter secured the bracelets to the forearm using two Velcro straps, following a procedure to match the tightness on the two arms. The experimenter first fixed the Velcro of one bracelet at a tightness sufficient to secure the bracelet, but not so tight as to cause discomfort. After the first bracelet was secured, the experimenter checked the marks on the Velcro straps (at 0.5 mm increments), and initially fixed the second bracelet at the same marks. After both Velcro straps were fixed on the second bracelet, the force measurements were checked and the Velcro of the second bracelet was adjusted if they differed of more than 0.1 N.

To reduce the effects of environment and actuator noise, the participants wore headphones playing white noise and the experimenter's instructions. This experiment was conducted during the COVID-19 pandemic with safety precautions such as social distancing, disinfecting the setup between each uses, and face masks.

1) Task: The experiment consisted of a number of trials where the participant verbally reported whether one of the stimuli felt more, less, or equally intense to the reference despite the difference in the actuation direction. Participants were indicated on a monitor which wrist received the fixed reference stimulus and which stimulus would be adjusted according to their response. After experiencing each stimulus pair, participants reported whether the adjusted stimulus should be increased (response 'more'), if it should be decreased (response 'less') or if it felt the same as the reference (response 'same'). Based on the participant's response, the actuator displacement for the adjusted stimulus was computed for the next trial using the staircase method and "twoup one-down" paradigm [29]. Fig. 7 shows an example trial with participant responses and actuator displacement of the adjusted stimulus. For iteration n, if the participant's response was 'more', the actuator displacement was computed as:

$$X(n) = X(n-1) * (10)^{(Ldb/20)}$$
(1)

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TABLE I

FLOW OF THE MAIN EXPERIMENT FOR EACH PARTICIPANT IN TERMS OF REFERENCE STIMULUS AND LOCATION OF EACH STIMULUS

	PHASE 1						PHASE 2			
	Stimulus location		Reference stimulus			Stimulus location		Reference stimulus		
	Left	Right	Training 1	Training 2	Test 1	Test 2	Left	Right	Test 3	Test 4
User 1, 5	Shear	Normal	Normal	Shear	Normal	Shear	Normal	Shear	Normal	Shear
User 2, 6	Shear	Normal	Shear	Normal	Shear	Normal	Normal	Shear	Shear	Normal
User 3, 7	Normal	Shear	Normal	Shear	Normal	Shear	Shear	Normal	Normal	Shear
User 4, 8	Normal	Shear	Shear	Normal	Shear	Normal	Shear	Normal	Shear	Normal

where X(n) and X(n-1) are the current and previous displacements and $Lbd = 4/(2^i)$ is the stimulus intensity. *i* is how many times the participant gave the 'less' response, such that with each 'less' response, the actuator displacement returned to the previous value (X(n) = X(n-2)) and *i* was increased by 1. When participants gave the response 'same', the algorithm computed the next iteration using the previous response in the sequence. This allows participants express that they perceive the stimuli to be equal, while allowing the staircase algorithm to overshoot the levels where both stimuli feel equally intense. The staircase was terminated if for the last 10 trials the average displacement change was less than 0.5 mm.

After each response, both the reference and the adjusted stimuli return to their neutral states (0 mm actuator stroke). To minimize the impact of actuation velocity or differences in duration on intensity evaluation, reference and adjusted stimuli were applied in sequence, as first the reference and the adjusted stimuli with 2-second pause in between. The experimenter verbally announced the reference and adjusted stimuli before actuation. In pilot testing, 3 mm was found to be an effective reference value for both stimuli because shear stimuli less than 3 mm were hard to notice and normal stimuli more than 3 mm caused discomfort/pain.

2) Preliminary Study: Comparing the Same Stimuli: Before conducting the main study to compare normal and shear stimuli, the proposed experiment and the method of adjustments were validated with a preliminary experiment, where participants wore haptic bracelets rendering the same type of stimuli on both wrists (normal-normal or shear-shear) and compared the intensity of the same stimuli. Half of the participants compared the normal stimuli first and the shear stimuli second, while the other half compared the shear stimuli first and the normal stimuli second.

For each participant, 1 training trial and 4 testing trials were performed with the first set of bracelets: the reference was given on the right arm during 2 testing trials and on the left arm during 2 testing trials. The order of the trials with reference stimulus on the right or left arm were changed for each user as well. Once the participant completed 4 testing trials, the same procedure was repeated with the second set of bracelets: normal bracelets were replaced with shear, and shear bracelets were replaced with normal. During all trials, the reference actuator displacement was set as 3 mm.

3) Main Study: Comparing Different Stimuli: Table I shows the experiment flow with two main phases: in the

Phase 1, the participant wore the bracelets as designated and performed two training and two testing blocks. In the Phase 2, the location of the bracelets were switched and the participant performed two more testing blocks. Participants familiarized themselves with the task during two training blocks. Each training block included one trial with a normal reference and one trial with a shear reference, both with a reference value of 3 mm. During the training blocks, the participants were encouraged to ask questions about the task. After the training blocks were performed, the experimenter made sure that all participants were confident with the task. Then, the testing blocks started.

Pilot tests revealed that the shear reference cannot be less than 3 mm to be noticed easily. Consequently, the participants compared normal and shear stimuli with (i) 1, 2, and 3 mm normal reference and (ii) 3 mm shear reference. The participants repeated each reference value 3 times. The order of the reference values were randomized for each testing block with normal reference. Participants received a 1-minute break after each set of 6 testing trials. Between Phase 1 and Phase 2, participants swapped the locations of bracelets (exchanging which arm received normal and shear stimuli), thus they received a longer break time of approximately 5 minutes including the preparation time.

B. Results

1) Preliminary Study: Comparing the Same Stimuli: Fig. 8(a,1) shows the average PSEs in terms of actuator displacements when the participants were asked to compare the same stimuli (normal-normal and shear-shear). Onetailed t-tests indicate that the mean PSEs are not statistically different for the normal stimulus adjusted to match the normal reference (t(15) = -0.6884, d = -1.7216, p = 0.517)and for the shear stimulus adjusted to match the shear reference (t(15) = -1.0121, d = -0.2531, p = 0.327). These results indicate the validity of the experiment and the ability of participants to compare stimuli intensities acting on the wrists.

2) Main Study: Comparing Different Stimuli: Actuator Displacements: PSEs were analyzed in terms of actuator displacements (mm), as shown in Fig. 8(a,2). Each bar represents the average PSE for the adjustable stimulus, and the horizontal dashed lines shows the reference value corresponding to each bar. The first (blue) bar shows the average normal PSE (1.9 mm) for 3 mm shear reference. The second (red) bar shows the average shear PSE (3.7 mm)

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Fig. 8. Results of Experiment 2, for point of subjective equality: (a) PSE of actuator displacements with (1) preliminary and (2) main studies. Red dashed lines show the reference values, blue boxes indicate normal PSEs, red boxes indicate shear PSEs with 3 mm reference, green box indicates shear PSEs with 2 mm reference, and orange box indicates shear PSEs with 1 mm reference. 'r' represents the actuator displacement for the reference stimulus. (b) A fit line model between actuator displacements of shear PSE and normal reference for each user. Labels are ordered based on the line slope.

for 3 mm normal reference. The third (green) bar shows the average shear PSE (2.7 mm) for 2 mm normal reference. Finally, the forth (orange) bar shows the average shear PSE (1.7 mm) for 1 mm normal reference.

Each participant performed 3 repetitions for each condition, and the PSEs were averaged and submitted to a twoway repeated-measure analysis of variance (ANOVA) with factors reference stimulus (1, 2, and 3 mm normal and 3 mm shear) and which arm was the reference applied to (dominant or non-dominant side). Mauchly's test ($\chi^2(5) =$ 1.991, p = 0.852) did not indicate a violation of sphericity. There was an influence of the value of the reference stimulus and type of reference on PSE (F(3, 56) = 42.994, p < 0.001, $\eta^2_{partial} = 0.697$). Most notably, single-sample t-tests indicate a difference between PSE and the displacement in the reference for all four conditions (p < 0.01). A post-hoc Tukey test showed that there was no difference in PSE between the 1 mm normal and 3 mm shear references stimuli, while all the other paired comparisons were significant, see Fig. 8(right). The main effect of the arm dominance was not significant $(F(1,56) = 1.197, p = 0.279, \eta_{partial}^2 = 0.021)$, indicating no consistent change in PSE whether the reference is applied to the dominant or non-dominant arm. The interaction effect was also not significant (F(3,56) = 0.733, p = 0.537, $\eta^2_{partial} = 0.038$), implying that the reference has the same effect no matter the arm dominance.

Fig. 8(b) shows the relationship between shear PSEs over normal reference intensities. Data for each participant and on average were modeled with a linear fit. We calculated a Pearson coefficient to observe the correlation between the data collected from the participants for each reference stimulus. We have found no correlation between participants for all reference stimulus, implying that all participants perceived the stimuli differently.

Interaction Forces: While participants were asked to

perceptually match the sensation produced by the two types of displacement, it is possible to analyse the stimuli both in terms of *displacements* (as we have done above) or in terms of the interaction *forces*. The recordings indicate that the forces in the non-actuated directions do not vary across trials, so only the forces in the actuated direction are discussed here. Fig. 9 shows the interaction forces recorded at the end of each trial during different references and averaged for all trials and participants.

A two-way ANOVA on the influence of two independent variables (stimuli type and reference) was conducted on the measured interaction forces. All effects were statistically significant at the 0.05 significance level. The main effect for stimuli type (normal vs. shear) yielded an *F* ratio of F(1,56) = 271.798, p < 0.001, $\eta_{partial}^2 = 0.829$, indicating that when participants thought that normal and shear stimuli intensities were equal, the interaction forces were statistically significantly different from each other. Similarly, the main effect for reference type gave an *F* ratio of F(3,56) = 42.389, p < 0.001, $\eta_{partial}^2 = 0.694$. The interaction effect was found as F(3,56) = 3.033, p < 0.037, $\eta_{partial}^2 = 0.140$. Interaction forces with normal and shear stimuli were statistically significantly different for all reference displacements.

A post hoc Tukey test showed that the PSE of interaction forces collected with the 2 mm normal reference and 3 mm shear reference were not statistically significantly different from each other, while all the other comparisons were statistically significantly different. For 2 mm normal reference and 3 mm shear reference, the PSE of actuator displacements on average were calculated as 2.76 mm and 1.9 mm, respectively. While the ANOVA results indicate that the PSEs of actuator displacements are statistically significantly different from each other, their average is somewhat similar. It is possible that such difference is caused by the fact that the PSEs of actuator displacements vary across people. So,

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Fig. 9. Measured interaction forces for Experiment 2 when the normal reference is given as 1, 2, 3 mm and shear reference is given as 3 mm. 'r' represents the actuator displacement for the reference stimulus.

even though on average the participants reached the same interaction forces with similar actuator displacements, how they individually perceive the applied forces can vary.

C. Discussion

Relative intensity of normal and shear stimuli based on actuator displacements. The PSEs showed that normal and shear stimuli can create the same intensity when shear stimuli had a larger displacement than normal (Fig. 8(a,2)), regardless of participant, reference stimulus type (normal/shear), reference stimulus intensity, or which wrist received the reference. This is possibly due to different mechanical properties of the skin or different mechanoreceptors involved.

These results support the subjective comments received from the study in Section III, but contradict the findings previously presented by Biggs et al. [27]. Since the main purpose of this experiment has been to support the subjective comments received from our wearable haptic bracelet, the main reasons for this contradiction has not been investigated deeply. Nevertheless, we believe that these reasons can be the differences between the actuator base or the probe diameter.

How the perceived intensity of normal and shear stimuli are affected by applied force. The force measurements (Fig. 9) showed that normal and shear stimuli can create similar intensities with different forces. For each participant, normal stimuli resulted in statistically significantly greater forces than shear stimulus needed to create a similar perceived intensity at the wrist. In other words, participants were more sensitive to shear forces compared to normal forces. Unlike the actuator displacements, interaction forces measured in this study show a similar trend to the findings of Biggs *et al.* [27]. (They estimated forces using the actuator displacements they collected from the participants and skin stiffness measurements reported by Diller *et al.* [26].) This indicates that participants can perceive force stimuli similarly, regardless of how the haptic device is grounded.

Does the point of subjective equality vary across people? ANOVA results with the main effect of participants indicate that the PSEs of actuator displacements are statistically significantly different for each participant. Even though some participants performed fairly similar to each other (see Fig. 8(b)), claiming a constant ratio between normal and shear stimuli for all users would be erroneous. Instead, the relationship between normal and shear stimuli should be obtained for each user with a calibration process before using the wearable haptic devices to perform virtual or telemanipulated tasks where the relative perception of normal and shear stimuli are important.

How perception of shear displacement intensity can be modeled with respect to normal displacements. Our results showed that PSE of actuator displacements with normal stimuli is much lower than shear stimuli, while interaction forces with normal stimuli is much greater than shear stimuli. This means that equalizing normal and shear stimuli in terms of actuator displacements or interaction forces would create a perceptual bias if, for example, normal and shear stimuli were used as sensory substitution for the same stimulus. In this study, we implemented a linear model (Fig. 8(b)) using three data points collected with different values of normal reference; more data points could be collected to obtain a more accurate relationship. We found that an offset displacement is needed for shear stimulus to create the same intensity when the normal stimulus is in the rest state (0 actuator displacement). This offset might be caused by how we secure the bracelets on the wrist. Both normal and shear bracelets are attached to the wrist through straps, which squeeze the wrist. Even though the normal stimuli applied on the wrist is perceived at a single point rather than the whole wrist, it is possible that the strap adds to the actuated normal stimulus given during the trials.

V. CONCLUSIONS

In this work, we analyzed the effects of rendering interaction forces to user's forearm near the wrist based on virtual interactions. The results of our experiments showed that normal displacements enabled participants to differentiate different stiffness levels significantly better than skin stretch - especially when the difference between virtual object stiffness values are large.

Even though all participants reported that haptic cues are easier to notice with normal displacements, some reported that they enjoyed skin stretch more because it was more "subtle and calm" compared to the normal forces. However, this may be due to larger forces being applied in the normal direction. Our second study to measure point of subjective equality investigated how to ensure that participants perceive normal and shear stimuli applied by wearable haptic bracelets equally, such that they can be used as haptic feedback to indicate interaction forces that occur in a virtual environment. The main result is that normal and shear stimuli cannot be equalized based on actuator displacements or interaction forces, but rather based on perceived stimuli intensity after a calibration.

In future work, we will compare task performance during virtual manipulation tasks while users perceive normal and/or shear haptic feedback. Such a comparison is possible only after we implement a calibration process based on the experimental procedure we presented in this work. We will also continue exploring the perceptual differences between wearable and grounded haptic devices.

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REFERENCES

- J. M. Suchoski, S. Martínez, and A. M. Okamura, "Scaling inertial forces to alter weight perception in virtual reality," in *IEEE International Conference on Robotics and Automation*, 2018, pp. 484–489.
- [2] D. Leonardis, M. Solazzi, I. Bortone, and A. Frisoli, "A 3-RSR haptic wearable device for rendering fingertip contact forces," *IEEE Transactions on Haptics*, vol. 10, no. 3, pp. 305–316, 2017.
- [3] S. B. Schorr and A. M. Okamura, "Fingertip tactile devices for virtual object manipulation and exploration," in *Proceedings of the Conference on Human Factors in Computing Systems (CHI)*, 2017, pp. 3115–3119.
- [4] M. Ernst and M. Banks, "Humans integrate visual and haptic information in a statistically optimal fashion," *Nature*, vol. 415, pp. 429–33, 2002.
- [5] M. A. Srinivasan, G. L. Beauregard, and D. L. Brock, "The impact of visual information on haptic perception of stiffness in virtual environment," in *ASME Winter Annual Meeting*, vol. 58, 1996, pp. 555–559.
- [6] I. Jang and D. Lee, "On utilizing pseudo-haptics for cutaneous fingertip haptic device," in *IEEE Haptics Symposium*, 2014, pp. 635– 639.
- [7] M. A. Baumann, K. E. MacLean, T. W. Hazelton, and A. McKay, "Emulating human attention-getting practices with wearable haptics," in *IEEE Haptics Symposium*, 2010, pp. 149–156.
- [8] R. Wang, F. K. H. Quek, D. G. Tatar, J. K. S. Teh, and A. D. Cheok, "Keep in touch: Channel, expectation and experience," in *Proceedings* of the Conference on Human Factors in Computing Systems (CHI), 2012, pp. 139–148.
- [9] H. Culbertson, C. M. Nunez, A. Israr, F. Lau, F. Abnousi, and A. M. Okamura, "A social haptic device to create continuous lateral motion using sequential normal indentation," in *IEEE Haptics Symposium*, 2018, pp. 32–39.
- [10] T. Nakamura, N. Nishimura, M. Sato, and H. Kajimoto, "Development of a wrist-twisting haptic display using the hanger reflex," in *Proceedings of the Conference on Advances in Computer Entertainment Technology*, 2014, pp. 33:1–33:5.

- [11] N. Dunkelberger, J. Sullivan, J. Bradley, N. P. Walling, I. Manickam, G. Dasarathy, A. Israr, F. W. Y. Lau, K. Klumb, B. Knott, F. Abnousi, R. Baraniuk, and M. K. O'Malley, "Conveying language through haptics: A multi-sensory approach," in *Proceedings of the ACM International Symposium on Wearable Computers (ISWC)*, 2018, pp. 25–32.
- [12] S. Song, G. Noh, J. Yoo, I. Oakley, J. Cho, and A. Bianchi, "Hot & tight: Exploring thermo and squeeze cues recognition on wrist wearables," in *Proceedings of the ACM International Symposium on Wearable Computers (ISWC)*, 2015, pp. 39–42.
- [13] Y. Zheng and J. B. Morrell, "Haptic actuator design parameters that influence affect and attention," in *IEEE Haptics Symposium*, 2012, pp. 463–470.
- [14] L. Meli, I. Hussain, M. Aurilio, M. Malvezzi, M. K. O'Malley, and D. Prattichizzo, "The hBracelet: A wearable haptic device for the distributed mechanotactile stimulation of the upper limb," *IEEE Robotics and Automation Letters*, vol. 3, no. 3, pp. 2198–2205, 2018.
- [15] S. Casini, M. Morvidoni, M. Bianchi, M. Catalano, G. Grioli, and A. Bicchi, "Design and realization of the CUFF - Clenching upperlimb force feedback wearable device for distributed mechano-tactile stimulation of normal and tangential skin forces," in *IEEE/RSJ International Conference on Intelligent Robots and Systems (IROS)*, 2015, pp. 1186–1193.
- [16] B. Stephens-Fripp, R. Mutlu, and G. Alici, "Applying mechanical pressure and skin stretch simultaneously for sensory feedback in prosthetic hands," in *IEEE International Conference on Biomedical Robotics and Biomechatronics (Biorob)*, 2018, pp. 230–235.
- [17] C. Tejeiro, C. E. Stepp, M. Malhotra, E. Rombokas, and Y. Matsuoka, "Comparison of remote pressure and vibrotactile feedback for prosthetic hand control," in *IEEE RAS EMBS International Conference on Biomedical Robotics and Biomechatronics (BioRob)*, 2012, pp. 521– 525.
- [18] J. D. Brown, J. N. Fernandez, S. P. Cohen, and K. J. Kuchenbecker, "A wrist-squeezing force-feedback system for robotic surgery training," in *IEEE World Haptics Conference*, 2017, pp. 107–112.
- [19] E. Pezent, A. Israr, M. Samad, S. Robinson, P. Agarwal, H. Benko, and N. Colonnese, "Tasbi: Multisensory squeeze and vibrotactile wrist haptics for augmented and virtual reality," in *IEEE World Haptics Conference*, 2019, pp. 1–6.
- [20] E. M. Young, A. H. Memar, P. Agarwal, and N. Colonnese, "Bellowband: A pneumatic wristband for delivering local pressure and vibration," in *IEEE World Haptics Conference*, 2019, pp. 55–60.
- [21] M. Raitor, J. M. Walker, A. M. Okamura, and H. Culbertson, "WRAP: Wearable, restricted-aperture pneumatics for haptic guidance," in *IEEE International Conference on Robotics and Automation*, 2017, pp. 427–432.
- [22] T. K. Moriyama, A. Nishi, R. Sakuragi, T. Nakamura, and H. Kajimoto, "Development of a wearable haptic device that presents haptics sensation of the finger pad to the forearm," in *IEEE Haptics Symposium*, 2018, pp. 180–185.
- [23] M. Sarac, A. Okamura, and M. di Luca, "Haptic sketches on the arm for manipulation in virtual reality," in *IEEE World Haptics Conference* (Work-in-Progress), 2019.
- [24] M. Sarac, A. M. Okamura, and M. di Luca, "Effects of haptic feedback on the wrist during virtual manipulation," in *IEEE Haptics Symposium (Work-in-Progress)*, 2020. [Online]. Available: https://arxiv.org/abs/1911.02104
- [25] F. Conti, F. Barbagli, D. Morris, and C. Sewell, "Chai: An opensource library for the rapid development of haptic scenes," in *IEEE World Haptics Conference*, 2005, pp. 21–29.
- [26] T. T. Diller, "Frequency response of human skin in vivo to mechanical stimulation," 2001.
- [27] J. Biggs and M. A. Srinivasan, "Tangential versus normal displacements of skin: Relative effectiveness for producing tactile sensations," in *Proceedings of Symposium on Haptic Interfaces for Virtual Envi*ronment and Teleoperator Systems, 2002, pp. 121–128.
- [28] X. A. Wu, S. A. Suresh, H. Jiang, J. V. Ulmen, E. W. Hawkes, D. L. Christensen, and M. R. Cutkosky, "Tactile sensing for gecko-inspired adhesion," in *IEEE/RSJ International Conference on Intelligent Robots* and Systems (IROS), 2015, pp. 1501–1507.
- [29] H. Levitt, "Transformed up-down methods in psychoacoustics," *The Journal of the Acoustical society of America*, vol. 49, no. 2B, pp. 467–477, 1971.

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