

Experimental and numerical studies on shear behaviour of macro-synthetic fibre reinforced prestressed concrete beams

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EXPERIMENTAL AND NUMERICAL STUDIES ON SHEAR BEHAVIOUR OF MACRO-SYNTHETIC FIBRE REINFORCED PRESTRESSED CONCRETE BEAMS

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ABSTRACT

Experimental and numerical studies on shear behaviour of macro synthetic fibre reinforced prestressed concrete (MSFRPC) beams are presented. MSFRPC beams are tested at a shear span to depth ratio (a/d) of 2.4 to understand the role of macro synthetic polyolefin fibres on the shear resistance and failure modes. The fibre volume fraction of 0.0%, 0.5%, 1.0% and 1.5% are considered as study parameters. A three-dimensional nonlinear finite element (FE) analysis is carried out to understand the influence of fibres on shear behaviour using the concrete damage plasticity model. Tensile constitutive relations of FRC is derived using inverse analysis from fracture test results and used as input in the FE model. A stage-wise analysis is conducted to include the effects of prestressing and applied external shear loads. The results from FE analysis showed a good agreement with experimental results for different fibre dosages. The effect of level of prestressing and varying compressive strength is studied through calibrated FE models. Due to the addition of macro synthetic fibres, no significant improvement in compressive strength is observed. Low fibre volume addition of 0.5% did not produce an appreciable improvement in shear behaviour. However, test and FE results of beams with higher volume fractions of 1.0% and 1.5% significantly improved the post-cracking behaviour, ductility, and ultimate shear resistance of MSFRPC beams.

Keywords: ABAQUS, Concrete damage plasticity, DIC, Shear, Prestressed concrete beams, Polyolefin fibres.

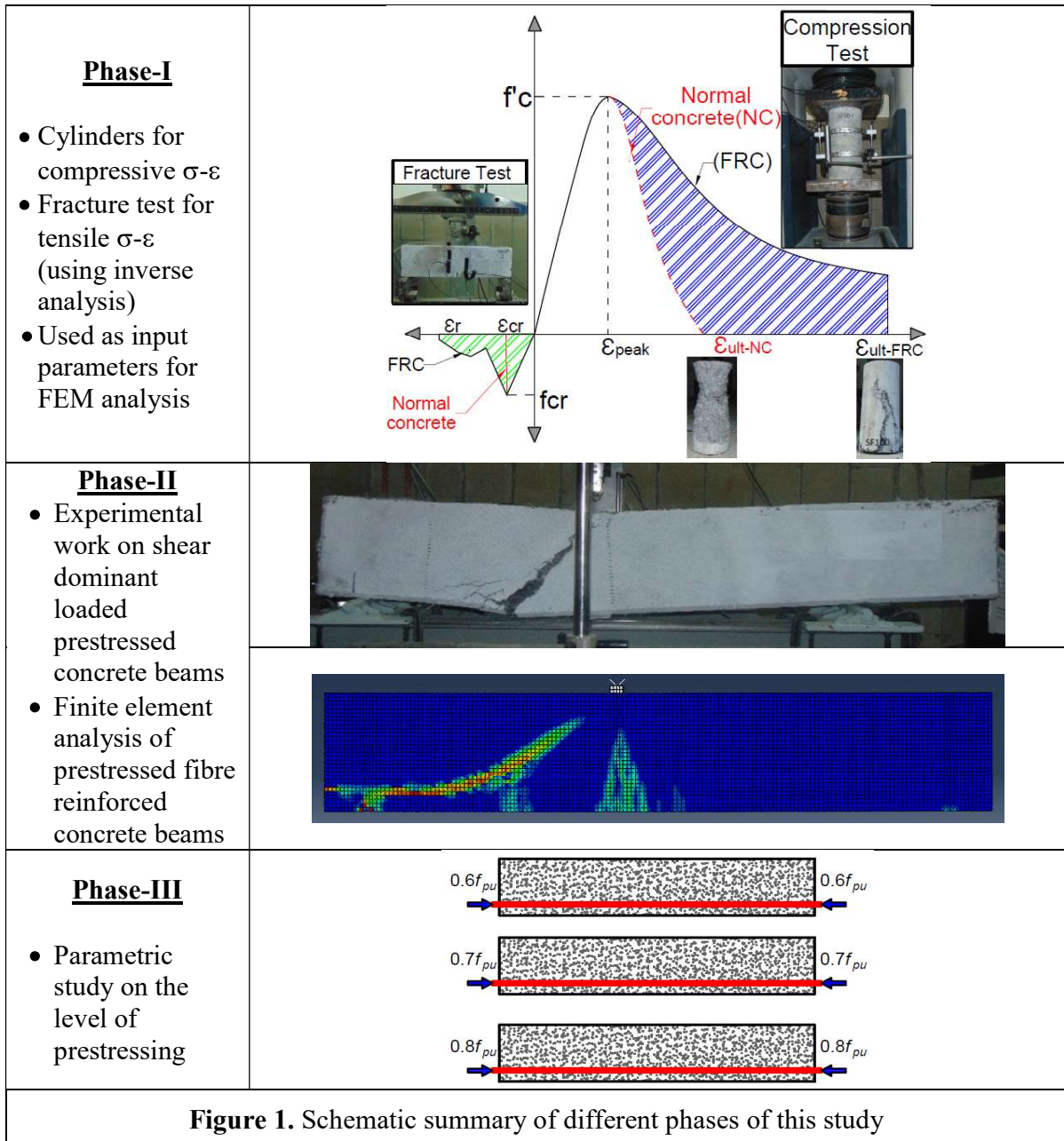
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31 **1.0 INTRODUCTION**

32 High-strength prestressed concrete (PC) beams are commonly used in various prestressing
33 applications [1–3]. Though the use of high-strength concrete has several advantages, it increases
34 the brittle behaviour of PC members. PC beams can fail in a brittle manner under shear dominant
35 loading [1,2,4–6]. The shear behaviour and failure modes of the PC beam depends on various
36 parameters such as compressive strength of concrete, longitudinal and shear reinforcement ratio,
37 level of prestressing, and level of flexure to the shear stress ratio at the critical section. This study
38 tries to understand the shear behaviour of macro-synthetic fibre reinforced prestressed concrete
39 (MSFRPC) beams. Adding discrete fibres in concrete can ensure adequate ductility of prestressed
40 concrete members under various loading conditions.

41
42 The use of fibre-reinforced concrete (FRC) in prestressing application can improve the ductile
43 performance by preventing crack progression. Previous studies on FRC highlighted the beneficial
44 effects of fibres on improving the performance of concrete at both the material and member level
45 [7–15]. ACI provisions [16] suggest a minimum of 0.75% of the volume fraction of steel fibres
46 for replacing the stirrups [15,17]. Lakavath et al. [18] previously investigated the influence of steel
47 and hybrid fibres on the shear behaviour of prestressed concrete beams. A significant improvement
48 in shear capacity was observed due to the addition of 0.5% and 1.0% volume fraction of steel
49 fibres. While the remarkable mechanical performance of steel fibre addition to concrete is
50 recognized, such a combination has durability issues. Steel is not only highly corrodible but also
51 costly to purchase, store and handle. Durability issues associated with SFRC have forced the
52 manufacturers and engineers to develop a variety of fibres with specific properties for
53 construction-related applications. Synthetic fibres such as polyolefin-based macro-synthetic fibre

54 types can solve the issues of reduced workability of FRC and corrosion without significantly
 55 compromising the structural performance. Studies in the past [19–25] have showcased that
 56 synthetic fibre reinforced concrete (SynFRC) is cost-effective in improving the tensile behaviour
 57 of concrete.



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4 59 Only a few authors in the past have focused on modifications of plasticity-based constitutive
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6 60 models [26]. The existing continuum plasticity damage model [27,28], such as the concrete
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9 61 damage plasticity (CDP) model, is used in this study. Only a few researchers in the past have used
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11 62 calibrated tensile constitutive behaviour of FRC in FEM simulations through inverse analysis [29].
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14 63 The schematic presentation of different phases involved in this study is shown in **Figure 1**. Phase-
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16 64 I includes the material characterization of FRC in compression and tension. Phase-II consists of
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19 65 experimental studies on prestressed concrete beams with different fibre dosages at shear span to
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21 66 depth ratio of 2.4 and validation with finite element analysis. Finally, Phase-III includes parametric
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24 67 studies.
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29 69 **2.0 RESEARCH SIGNIFICANCE**

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31 70 Only minimal information exists on the behaviour of macro synthetic fibre-reinforced prestressed
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34 71 concrete beams subjected to shear dominant loads. Thus, macro-synthetic fibres reinforced
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36 72 prestressed concrete beams are tested under shear dominant loading ($a/d=2.4$ to fill the existing
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39 73 knowledge gap. Besides, fracture tests are conducted as well to understand the role of fibres in
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41 74 crack arresting. The main parameter considered in this study are different volume fraction of fibres
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43 75 such as ($V_f = 0.0\%$, 0.5% , 1.0% and 1.5%). However, all other parameters such as compressive
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46 76 strength, dimensions of beam, and shear span to depth ratio are kept constant. The key observations
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48 77 due to the addition of fibres include variations in ductility, toughness, failure mode, and capacity
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51 78 of beams. Hence, the specific objectives of the present study are:

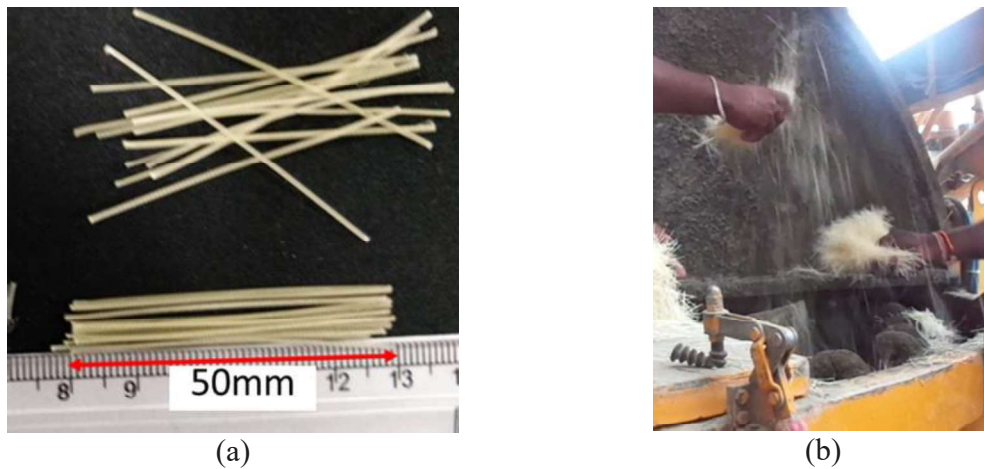
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53 79 1. To understand the effectiveness of macro-synthetic fibres in improving the shear behaviour
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55 80 of prestressed concrete beams by carrying out experimental studies.

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4 81 2. To monitor the crack initiation and its propagation in notched prism beams and full-scale
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7 82 prestressed concrete beams using digital image correlation technique (DIC).
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9 83 3. To utilize the multi-linear stress-strain model (based on fracture tests) as an input for the
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11 84 nonlinear finite element analysis to simulate the shear behaviour of MSFRPC beams.
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14 85 4. To carry out parametric studies on the influence of level of prestressing force on the shear
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16 86 behaviour of MSFRPC beams.
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21 88 **3.0 EXPERIMENTAL PROGRAM**

23 89 Pretensioned beams of dimensions 150 mm x 300 mm x 1600 mm were cast in the precast factory
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26 90 and tested in heavy structures lab at the Indian Institute of Technology Hyderabad. Eight beams
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28 91 were tested at a shear span to depth (a/d) ratio of 2.4. As per Kani's classical theory [30], the a/d
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30 92 ratio of 2.5 is the transition point below which the RC beams fail in a shear critical mode.
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33 93 Therefore, a/d ratio of 2.4 is considered in this study to avoid arch action and ensure diagonal shear
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35 94 tension (DST) mode [31,32]. The variables considered in this study are 0.0%, 0.5%, 1.0% and
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38 95 1.5% of volume fraction (V_f) of macro-synthetic fibres (MSF). In this study, MSF100 represents
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40 96 prestressed concrete beams reinforced with macro synthetic fibres of 1.0% by concrete volume.
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43 97 The concrete mix was designed to attain a strength of 50 MPa as per the Indian standard IS 10262
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45 98 [33]. The design concrete mix includes the fine aggregates, coarse aggregate, cement,
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47 99 superplasticizer, and water content as detailed in **Table 1**. All the materials were added in the
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50 100 following sequence to avoid the balling effect. Firstly, the total quantity of coarse aggregates, fine
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52 101 aggregates, and cement was added, followed by 50% of the total water quantity. Afterwards, macro
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54 102 synthetic fibres were added manually, as shown in **Figure 2(b)**. Finally, the remaining water and
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56 103 superplasticizers were added to the pan mixture. Details of fibre and manual addition of fibres to
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4 104 the concrete while mixing is shown in **Figure 2**. The obtained target cube compressive strength is
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6 105 58 MPa. In the same mix, the fibre volume of 0.5% (4.55 kg/m³), 1.0% (9.1 kg/m³) and 1.5%
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8 106 (13.65 kg/m³) were added. The compressive strength of concrete cubes are 59 MPa, 67 MPa and
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10 107 68 MPa, respectively. The properties of the macro-synthetic fibres in this study are shown in **Table**
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14 108 **2**.



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37 110
38 111 **Figure 2.** Macro synthetic fibers (MSF) (a) Geometry (b) Mixing of MSF to concrete

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47 113 **Table 1.** Concrete mix proportion in kg/m³

Cement	CSS	NRS	Coarse aggregate		SP	Water	Macro-synthetic fibre (MSF) ($V_f = 0\%, 0.5\%, 1.0\%$ and 1.5%)
			20 mm	10 mm			
450	415	312	755	355	2.6	152	0.0, 4.55, 9.1 and 13.65

Note: CSS= Crushed stone sand, NRS= Natural River Sand, SP= Super Plasticizer

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65 **Table 2.** Properties of macro-synthetic fibre (Polyolefin fibres)

Specification	Macro-synthetic fibre (MSF)
Specific gravity	0.91
Length (mm)	50
Diameter (mm)	0.5
Tensile strength (MPa)	618
Modulus of elasticity (GPa)	10
Aspect ratio	100

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4 114 **3.1 Compression Tests on Concrete Cylinders**

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7 115 Concrete cylinders of size 150 mm (diameter) x 300 mm (length) were tested under uniaxial
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9 116 compression to understand the effect of macro synthetic fibres in improving the strength and
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11 117 ductility. All the cylinders were tested in displacement control mode with a rate of 1 mm/min,
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14 118 using a servo-controlled compression testing machine of 500 kN capacity. Three linear variable
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16 119 displacement transducers (LVDT) are attached to cylinders for monitoring the axial deformation.
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19 120 Average compressive stress-strain curves are shown in **Figure 3**. Test results revealed that the
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21 121 addition of fibres does not significantly influence the cylinder compressive strength. However, the
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23 122 compressive toughness index increased from 1.4 to 5.7 times due to the addition of macro synthetic
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25 123 fibres (**Table 3**). The toughness of MSF50 increased by 40% when compared to control cylinders
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28 124 due to the addition of 0.5% fibre volume dosage. However, the ultimate strain of MSF50 did not
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31 125 increase as that of MSF100 and MSF150 (**Figure 3**). In MSF50 specimens, the crack bridging and
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33 126 passive confinement offered by fibres was not effective to significantly increase the post-peak
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36 127 behaviour. Hence, the increment in toughness was not significant compared to higher dosages. The
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38 128 failure modes of cylinders due to the addition of fibres are shown in **Figure 3**. The peak
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41 129 compressive strength of the cylinder is in the range of 52 MPa - 54 MPa.
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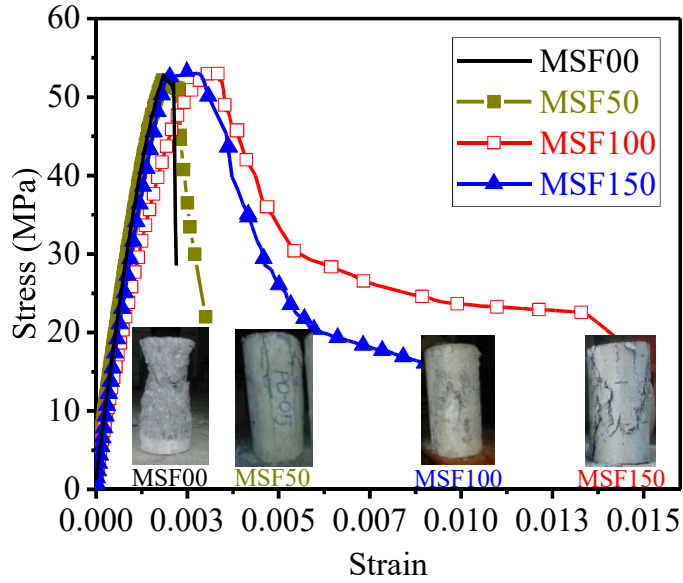


Figure 3. Stress-strain curve of concrete cylinders in compression

Table 3. Properties of MSFRC in Compression

Mix ID	Cube strength (MPa)	SD (MPa)	Cylinder strength (MPa)	SD (MPa)	Toughness (A_f)	Toughness index (T.I = A_f/A_c)
MSF00	57.91	1.46	52.75	1.05	0.0738	1.00
MSF50	59.23	1.30	53.46	1.26	0.1028	1.40
MSF100	67.08	1.27	53.62	0.83	0.2805	3.80
MSF150	68.12	1.18	54.14	1.10	0.4239	5.74

Note: SD = Standard deviation (MPa), A_f = area of the stress-strain curve of the fibre-reinforced concrete cylinder, A_c = area of the stress-strain curve of the control cylinder

The tension stiffening response of fibre reinforced concrete depends on the characteristics of fiber such as aspect ratio, length, types, the volume fraction of fibers, as well as matrix properties such as strength and aggregate size. Few researchers [34–39] in the past have studied the influence of fibre orientation factor on the mechanical performance of FRC, such as strength, load-CMOD, and fracture energy. They noted a considerable improvement in post-peak response due to the orientation effect [34,37,40]. The increment in post-peak response leads to an increase in residual flexural tensile strength (f_R). Thus, the ductility of fibre-reinforced prestressed concrete beams can

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4 143 be increased in both flexure and shear dominant loading. However, the effect of fibre orientation
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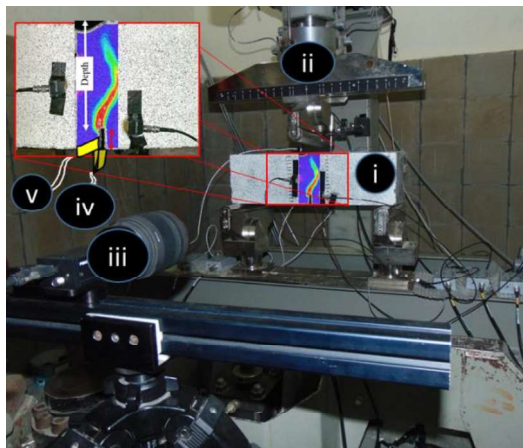
10 11 146 **3.2 Fracture Tests**

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14 147 Concrete prisms were cast and tested under a three-point bending test as per EN14651 (2005). The
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16 148 size of the prism is 150 mm x 150 mm x 500 mm. A notch of 25 mm depth and 5 mm width was
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19 149 prepared in the prism to localize the damage in a defined position. The crack width is monitored
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21 150 by crack mouth opening displacement (CMOD) and crack tip opening displacement (CTOD)
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24 151 gauges. Similarly, one LVDT is used to monitor the vertical deflection of the prism. A non-contact
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26 152 digital image correlation (DIC) technique was used to monitor full-field strain measurements and
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29 153 to study crack propagation. The DIC system consists of two light sources, one high-resolution
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31 154 camera, and a storage device, as shown in **Figure 4 (a)**. In the pre-processing phase, the notched
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34 155 beams were painted and speckled with black colour ink with a speckling gun [41]. After mounting
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36 156 all the gauges, the calibration image is captured before the start of testing. After that, images were
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39 157 captured at specific intervals according to the rate of loading. All the FRC prisms were tested under
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41 158 displacement control mode with a 5mm/min rate by using a flexure testing machine, as shown in
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43 159 **Figure 4 (a)**.

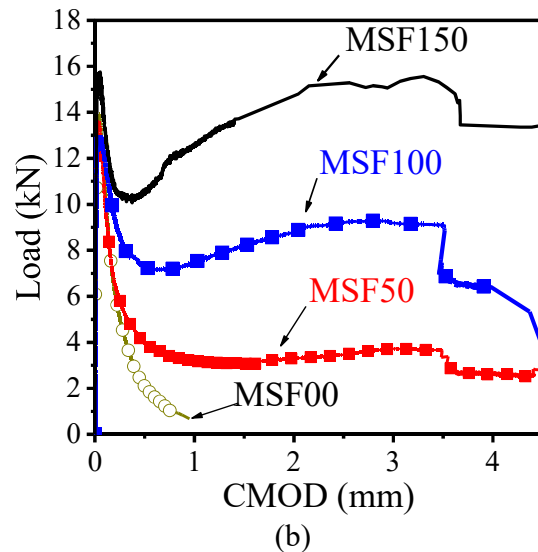
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48 161 The load-CMOD response of MSF00, MSF50, MSF100, and MSF150 concrete prisms are
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51 162 presented in **Figure 4 (b)**. The response shows that the post cracking behaviour was significantly
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53 163 improved due to the addition of 0.5%, 1.0%, and 1.5% of volume fractions of MSF compared to
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56 164 control (MSF00) beams. In control prisms (MSF00), the obtained peak load is 14 kN, which is the
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58 165 same as that of the MSF100 prism. However, MSF100 prisms also had a second peak load of 9.31

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4 166 kN, which occurred at CMOD of 2.3 mm. Thus, macro synthetic fibre addition did not change the
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7 167 first cracking load but significantly improved the post cracking behaviour. Similarly, in MSF50
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9 168 beams, the second peak load of 4kN is observed at a CMOD of 2.5 mm. Hence, from this
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11 169 experimental response, it is concluded that the MSF fibres of aspect ratio 100 can effectively
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14 170 engage in strain redistribution at higher crack openings such as 2.5 mm of CMOD. The load-
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16 171 CMOD curves were used to obtain the tensile stress-strain response from the inverse analysis. The
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19 172 multi-linear tensile stress-strain behaviour of specimens with different fibre volume fractions was
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21 173 obtained from the inverse analysis. More information on inverse analysis can be found elsewhere
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43 i. Test Specimen, ii. FTM Actuator, iii. DIC Camera,
44 iv. CTOD Gauge, v. CMOD Gauge



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(a) (b)
Figure 4. Fracture tests on MSFRC Prisms (a) Test setup, (b) Load-CMOD curve

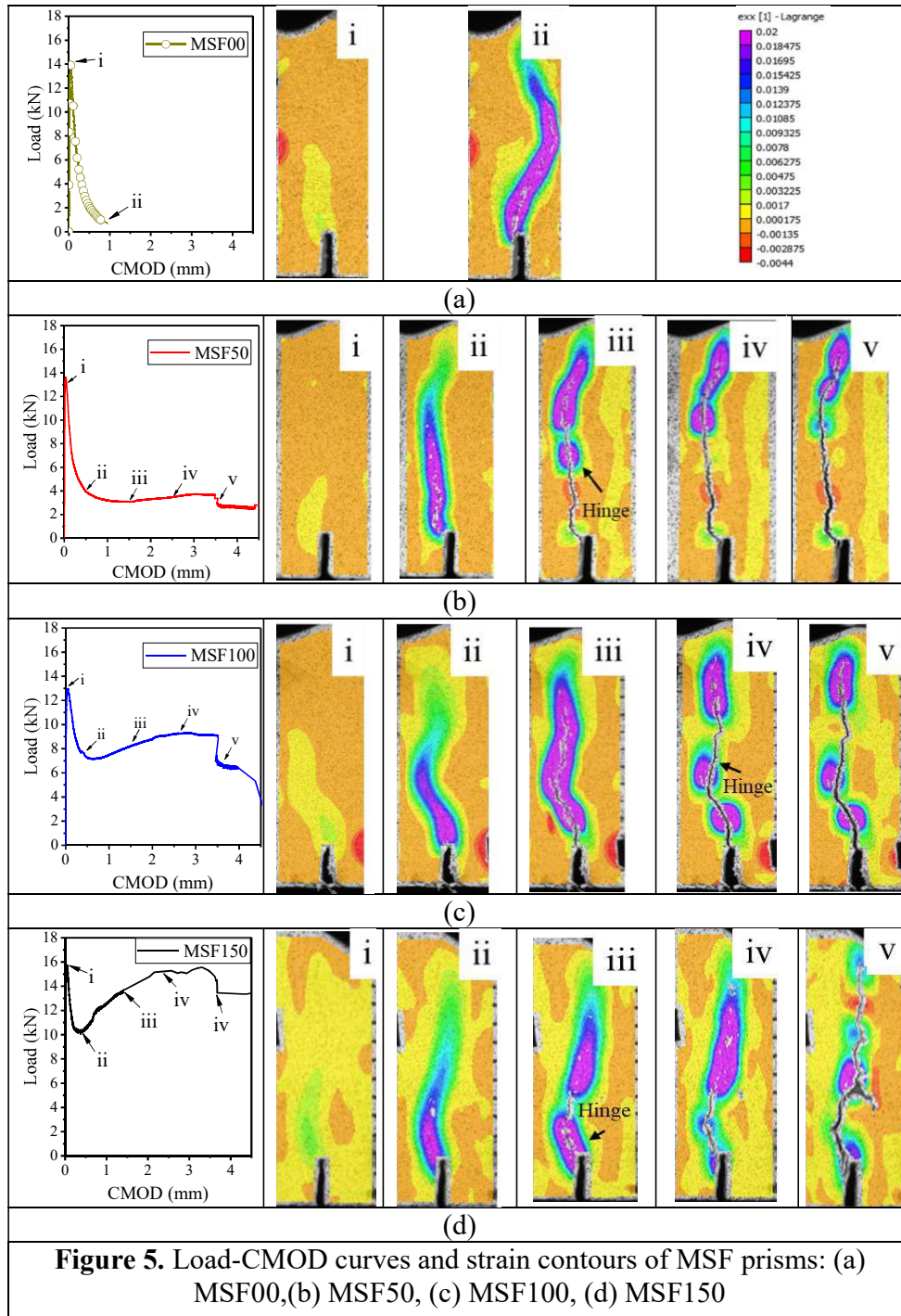
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177 The average residual flexural tensile strength (f_{R1} to f_{R4}) of MSFRC prisms was calculated based
178 on RILEM recommendation [43]. Here, f_{R1} , f_{R2} , f_{R3} , and f_{R4} are calculated at CMOD of 0.5mm,
179 1.5mm, 2.5mm, and 3.5mm respectively. The fracture energy (G_f) of prisms was calculated based
180 on the provisions of the Japan concrete institute (JCI) code [44]. The improvement in fracture
181 energy due to the addition of 0.5%, 1.0%, and 1.5% volume fraction of MSF fibres are 4.55, 9.62,

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4 182 and 16.03 times that of the control prism (MSF00). The residual flexural tensile strength of MSF
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7 183 prism was calculated based on the RILEM [43] recommendations and presented in **Table 4**. The
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9 184 DIC strain contours were used (**Figure 5**) for understanding the crack initiation and crack
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11 185 propagation at different CMOD values[21].
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17 **Table 4.** The residual flexural tensile strength and fracture energy of prisms

Mix ID	Residual flexural tensile strength (MPa)				Total fracture energy (N-mm)	The ratio of Fracture Energy (ΔG_f)
	f_{R1}	f_{R2}	f_{R3}	f_{R4}	$G_f (\times 10^{-3})$	$\Delta G_f = \frac{G_f}{G_{fc}}$
MSF00	0.69	-	-	-	156.7	1.00
MSF50	1.14	0.88	1.00	0.97	713.2	4.55
MSF100	2.10	2.36	2.65	2.62	1506.7	9.62
MSF150	3.04	4.00	4.39	4.34	2512.5	16.03

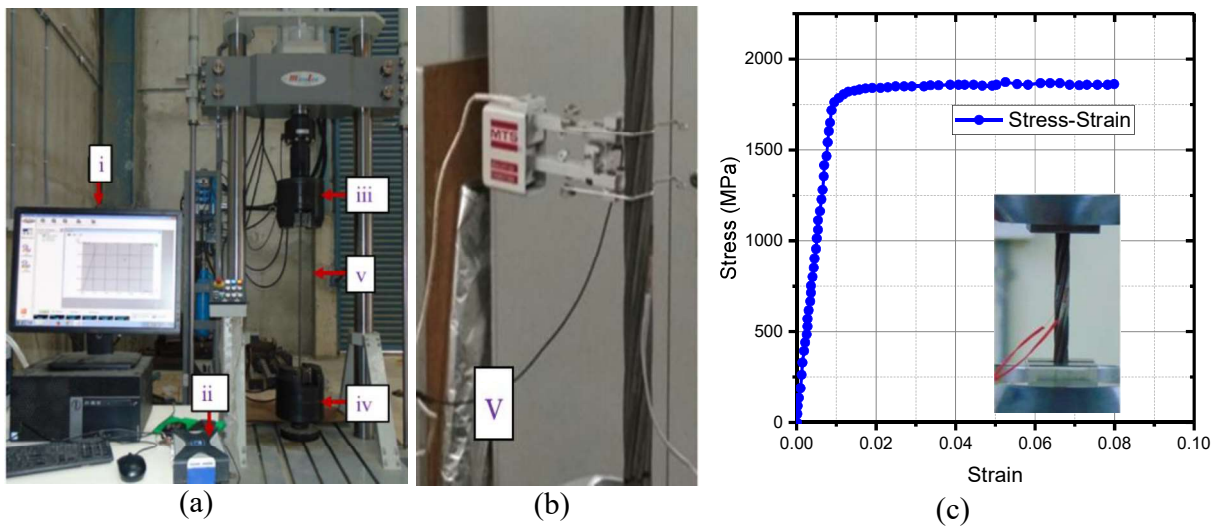
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33 189 In control prisms (MSF00), the crack propagated without the formation of any strain localization,
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36 190 as shown in **Figure 5 (a)**. However, in the case of MSF50 beams, the strain localization started at
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38 191 a CMOD of 1.5 mm. Similarly, in MSF100 beams, the number of hinge formations was more
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41 192 along the cracked surface compared to MSF50 beams. The crack initiated and propagated in MSF
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43 193 beams from the tension zone to the loading point progressively, and the propagation of the tip of
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46 194 the crack can be visualized in **Figure 5**. The strain contours from DIC analysis help understand
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48 195 the reason for a significant increase in the second peak in loading **Figure 4 (b)-(d)**. The hinges
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50 196 formed along the depth of the beam due to the bridging action of fibres against the crack opening,
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53 197 as shown in **Figure 5**. The detailed discussion about the formation of hinge and comparison with
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55 198 different fiber dosages were discussed in the previous work of authors [21].
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3.3 Stress-Strain Curve of Prestressing Strand

The seven-wire low relaxation prestressing strand of 12.7 mm diameter was tested under tension to get the stress-strain response. An extensometer and strain gauges were mounted to measure the

strains, as shown in **Figure 6 (b)**. The test is performed according to ASTM A1061 [45] with the help of a servo-controlled fatigue testing machine (FTM) as shown in **Figure 6**. The obtained stress-strain response of prestressing strand is shown in **Figure 6 (c)**. The average tensile strength of the prestressing strand is 1860 MP with an elastic modulus of 196 GPa (**Table 5**). The same test results were used for nonlinear finite element analysis simulation after converting the engineering stress-strain curve to the true stress-strain curve.



i-monitor, ii=Data acquisition system, iii=Upperlimb, iv=Lowelimb, v=Prestressing strand with clip-gauge

Figure 6. Coupon test of HTS strand: (a) Fatigue testing machine, (b) Extensometer, (c) Prestressing strand stress-strain curve

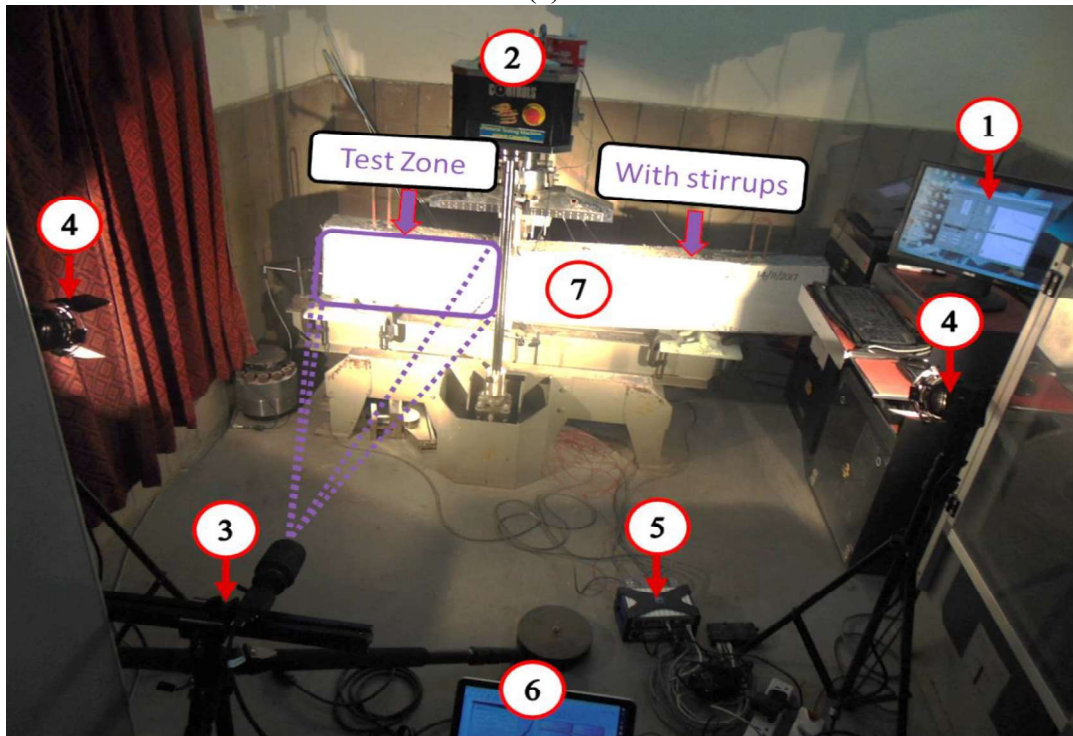
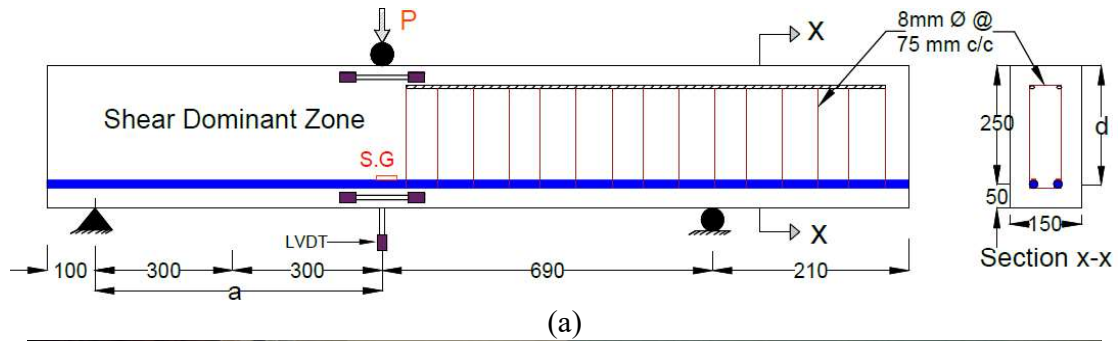
Table 5. Mechanical properties of prestressing strand

Avg. Tensile strength (MPa)	f_{yp}	1860
Area of cross-section (mm ²)	A_p	98.4
Modulus of elasticity (MPa)	E_p	196500
Poisson's ratio	γ	0.3

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4 213 **3.4 Testing of Prestressed Concrete Beams**

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6 214 The prestressed concrete beams of size 150 mm × 300 mm × 1600 mm were cast with MSFRC
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9 215 concrete (0.0%, 0.5%, 1.0% and 1.5% V_f of macro-synthetic fibers). In total, eight prestressed
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11 216 concrete beams were tested under shear-dominated loading, as shown in **Figure 7**.
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52 1. Controller, 2. Test frame of 300kN capacity, 3. DIC camera, 4. The light source, 5. Data Acquisition
53 system (DAC), 6. DAC data storage (DAC+DIC) and 7. Specimen
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55 (b)

56 **Figure 7.** Prestressed concrete beam details along with (a) Instrumentation, (b) Test setup

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4 219 Two LVDTs were used at the loading point for monitoring the deflection of beams. The strain in
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7 220 strands is monitored using strain gauges bonded on the prestressing strand. The level of
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9 221 prestressing applied in these beams is 40% to that of the ultimate capacity of the prestressing strand
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11 222 (1860 MPa). A prestressing force of 154.5 kN was applied at an eccentricity of 100mm. Due to
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14 223 this, average compressive stress of 3.43 MPa is produced. A DIC setup was used for tracking the
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16 224 crack initiation and propagation and for strain measurements in the test zone. The images of
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19 225 deformed specimens are captured at the same rate of loading in the shear dominant zone of the
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21 226 specimen. After that, post-processing is carried out by using VIC-2DTM package. All the
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24 227 prestressed concrete beams were tested using displacement control mode at a rate of 0.025mm/sec.
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26 228 In each series, two prestressed concrete beams were tested to ensure the consistency of test results.
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30 31 230 **4.0 TEST RESULTS AND DISCUSSION**

32 33 231 **4.1 Control beam (MSF00)**

34 232 The complete load-deflection response of macro synthetic fibre-reinforced prestressed concrete
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36 233 (MSFRPC) beams are shown in **Figure 8**. The first shear crack in MSF00 was initiated at a load
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39 234 of 178 kN and deflection of 2.9 mm (**Figure 9**). By strain contours from DIC measurements, the
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42 235 crack initiation and propagation path can be identified. MSF00 reached a peak load of 216.3 kN at
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45 236 a deflection of 4 mm. After reaching the peak load, a shear crack formed at an angle of 41.2° due
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48 237 to diagonal shear tension. The energy absorption capacity is calculated as the area under the load-
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51 238 deflection curve up to the ultimate load point. The ultimate load (P_u) point is considered as a 20%
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53 239 drop from the peak load (P) [18]. The average energy absorption capacity of the control beam is
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55 240 measured as 785.8 (kN-mm), and the failure mode is observed as direct shear tension (*DST*).
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4.2 MSFRPC beams (MSF50)

The load-deformation behaviour of the MS50 beam with a volume fraction of 0.5% is shown in **Figure 8**. The peak load of MSF50 was 264.6 kN at the deflection of 4.8 mm. The peak load increased by 21.4% when compared with a control beam (MSF00). The first shear crack initiated in MSF50 beams at a load of 160.6 kN at a deflection of 2.1 mm (**Figure 9**). MSF50 reached a peak load of 264.6 kN at a deflection of 4.8 mm, and shear crack is formed at an angle of 45.8°. The average energy absorption capacity of the MSF50 beam is obtained as 2918.2 kN-mm, which is 3.72 times more than that of control beams. A low fibre dosage of 0.5% could not change the failure mode, and MSF50 failed in direct shear tension failure mode.

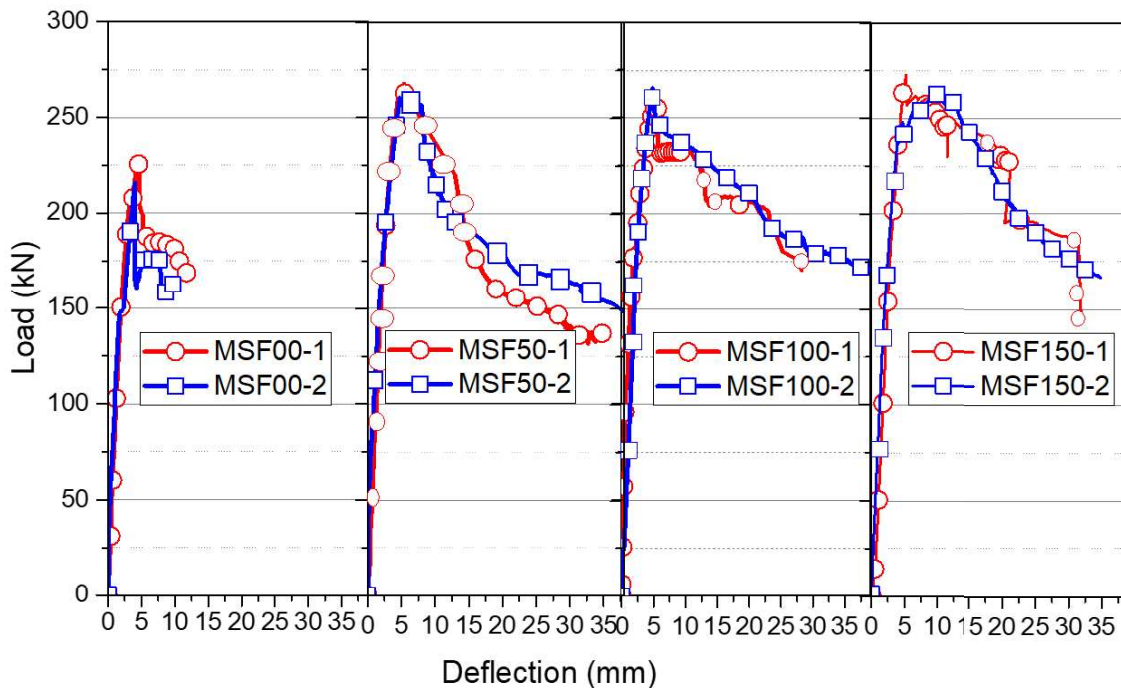
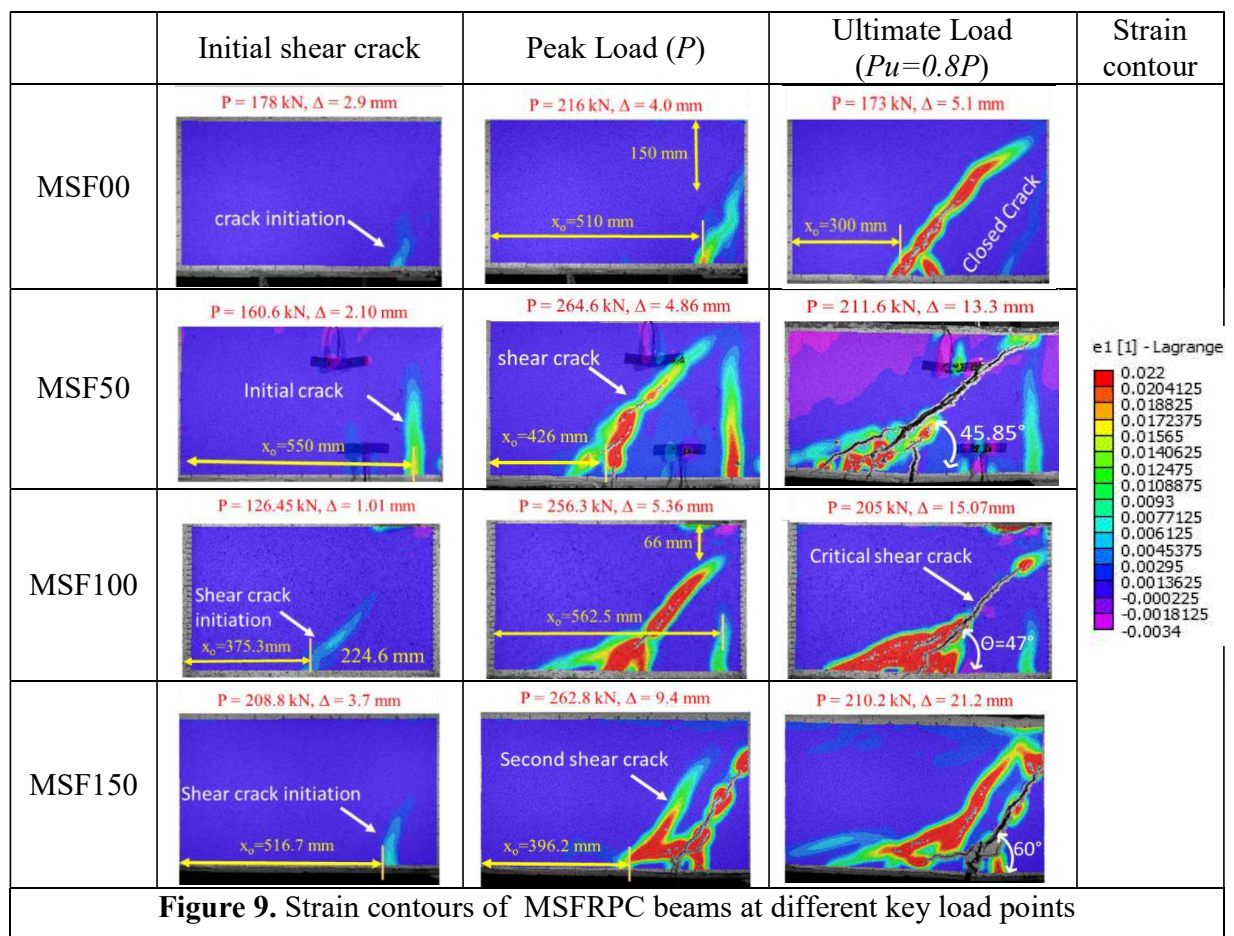


Figure 8. Load-deflection response of PO00, PO50, PO100, and PO150 beams

4.3 MSFRPC beams (MSF100)

The shear crack in MSF100 was initiated at a distance of 375.3 mm from the support (**Figure 9**). The same crack propagated towards the loading point with an angle of 47°. The improvement in

255 peak load is 40 kN to that of control beams (216 kN). This increase in peak capacity is due to the
 256 fibre bridging action, which restrained the crack opening. Similarly, the improvement in ultimate
 257 load is about 21.2% to that of the control beam. The strain contour plots of MSF100 beams (**Figure**
 258 **9**) showed more distributed cracks occurred at peak and ultimate load due to the presence of fibres.
 259 Also, the failure angle did not change much even with the addition of high fibre dosage. However,
 260 MSF100 beams failed in the ductile mode, as shown in **Figure 9**.



262 Energy absorption capacity (EAC) also increased significantly due to fibre addition (**Table 6**). The
 263 improvement in EAC due to the addition of 1.0% of macro synthetic fibres is 4.0 times that of
 264 control beams. A significant increase in EAC indicates the addition of fibres helps in absorbing
 265 the sudden energy release (control beams) and thereby converts the brittle failure to ductile mode.

4.4 MSFRPC beams (MSF150)

The MSFRPC beams reinforced with a 1.5% volume fraction of macro synthetic fibres reached a peak load of 272.7 kN. Also, the improvement in EAC is 6.0 times that of control beams. The fibres contributed effectively to strain redistribution, due to which the post-peak response increased reasonably. Similarly, the ultimate load improvement is about 26% to that of the control beam is observed. From the strain distribution plots of MSF150 beams, it is observed that more distributed cracks occurred along with new shear cracks at peak and ultimate load. Moreover, due to the higher dosage of fibre addition, the crack angle of the critical crack increased from 41° to 65°. MS150 beams failed in ductile mode, as shown in **Figure 9**. From experimental results, it is observed that the beam reached its ultimate load at the deflection of 21 mm (**Table 6**).

Table 6. Summary of test results of MSFRPC Beams

Beam ID		A	B	C	D (kN-mm)	θ (°)	Failure mode
MSF00-1	Load (kN)	178	216.3	173.0	785.8	41.2	DST
	Δ (mm)	2.9	4.0	5.1			
MSF00-2	Load (kN)	167	224.5	179.6	741.5	42.4	DST
	Δ (mm)	2.6	4.2	5.3			
MSF50-1	Load (kN)	160.6	262.6	211.6	2918.2	45.8	DST
	Δ (mm)	2.1	4.8	13.3			
MSF50-2	Load (kN)	158.8	260.2	208.2	2298.8	45.0	DST
	Δ (mm)	2.6	4.7	10.9			
MSF100-1	Load (kN)	126.5	256.3	205.0	3183.5	47.5	DST
	Δ (mm)	1.0	5.3	15.0			
MSF100-2	Load (kN)	131.2	262.2	209.7	3184.8	49.3	DST
	Δ (mm)	1.2	5.4	15.2			
MSF150-1	Load (kN)	159.2	272.7	218.2	4742.8	65.3	FS
	Δ (mm)	2.5	5.3	21.4			
MSF150-2	Load (kN)	208.8	262.8	210.2	4733.7	60.2	FS
	Δ (mm)	3.7	9.4	21.2			

Note: A = Shear crack load (kN), B = Peak load (kN), C = Ultimate load (kN), D = Energy absorption capacity (EAC) (kN-mm), θ = Failure crack angle, DST= Direct shear tension, FS=Flexure shear.

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4 283 **4.5 Discussion**

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7 284 The control prestressed concrete beams cracked at a distance of 510 mm from support. After peak
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9 285 load, the new crack is initiated at a distance of 300 mm from support, as shown in **Figure 9**, and
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11 286 the beam collapsed in brittle mode. However, MSF50 beams with 0.5% volume fraction, a flexural
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13 287 crack initiated at a distance of 550 mm from support. At peak load point, it cracked in shear at a
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15 288 distance of 426 mm from support and led to final failure under direct shear tension mode. Similarly,
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17 289 the MSF100 beams with 1.0% of fibre volume fraction had a shear crack at a distance of 375.3
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19 290 mm from support but did not fail in a brittle manner. The MSF150 beams had a flexure-shear crack
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21 291 at a distance of 516.7 mm. With the increase in applied loads, the same crack propagated towards
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23 292 the loading point at an angle of 60°. Other than MSF100 beams, the critical crack initiation length
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25 293 increased with an increase in fibre volume fraction. Similarly, the crack propagation rate reduced
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27 294 with an increase in the dosage of fibres.
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36 296 After the failure of specimens, the fibre distribution in a cracked plane is measured to understand
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38 297 the nature of fibre distribution. The failure plane of prestressed fibre reinforced concrete beams
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40 298 was divided into several grids, as shown in **Figure 10** with an offset of 50 mm in both horizontal
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42 299 and vertical directions. The fibre distribution in MSF50 was 65 to 75 numbers in a 50 mm grid.
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44 300 Similarly, in both MSF100 and MSF150 beams, the number of fibres across the cracked plane
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46 301 increased significantly, as shown in **Figure 10 (b)**. Fibre distribution was found to be even across
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48 302 the depth of the failure plane. Both the rupture and pull-out failure of fibres were observed.
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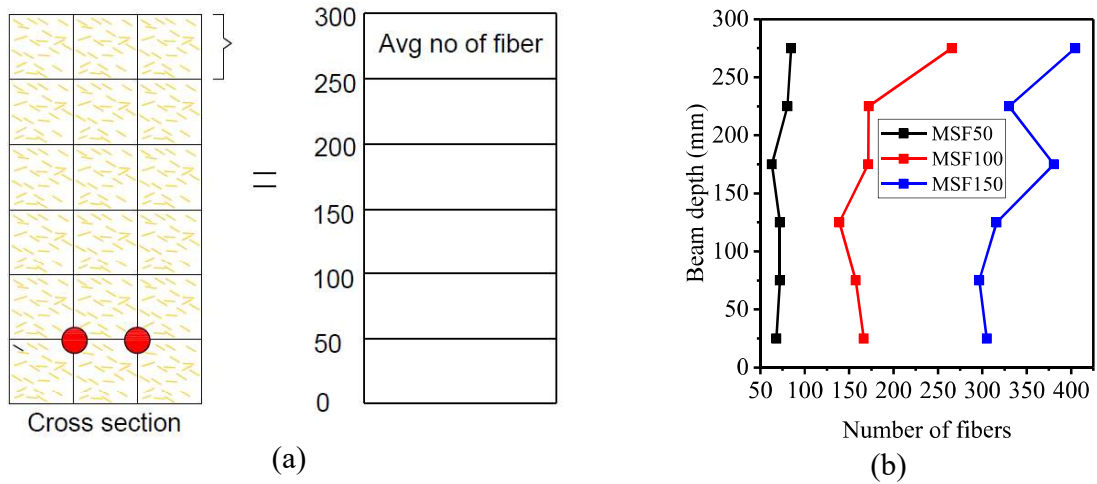


Figure 10. Fibre distribution across the depth of MSFRPC beam: (a) Grid with 50 mm x 50 mm spacing, (b) Average number of fibres across the depth

5.0 FINITE ELEMENT STUDIES

Three-dimensional FE models of test beams were created using finite element software ABAQUS. Concrete is modelled using C3D8R element with concrete damage plasticity model (CDP) as a material model. The prestressing strand and steel reinforcement were modelled using the truss element (T3D2). The stage-wise analysis is performed for prestressing and the applied shear loading.

5.1 Material Properties

Test specimens had an average compressive strength of 54 MPa, and the same is used for FE model. The stress-strain response of high-strength concrete without fibres in compression is modelled using the Thorenfeldt model[46]. Similarly, the stress-strain response of fibre reinforced concrete under compression is modelled using Yu-Chen et al. [47] model. The tension-stress strain behaviour is obtained from the inverse analysis developed by Bhosale et al. [42]. The stress-inelastic strain in both compression and tension for FRCs with different fibre dosages are shown in **Figure 11**.

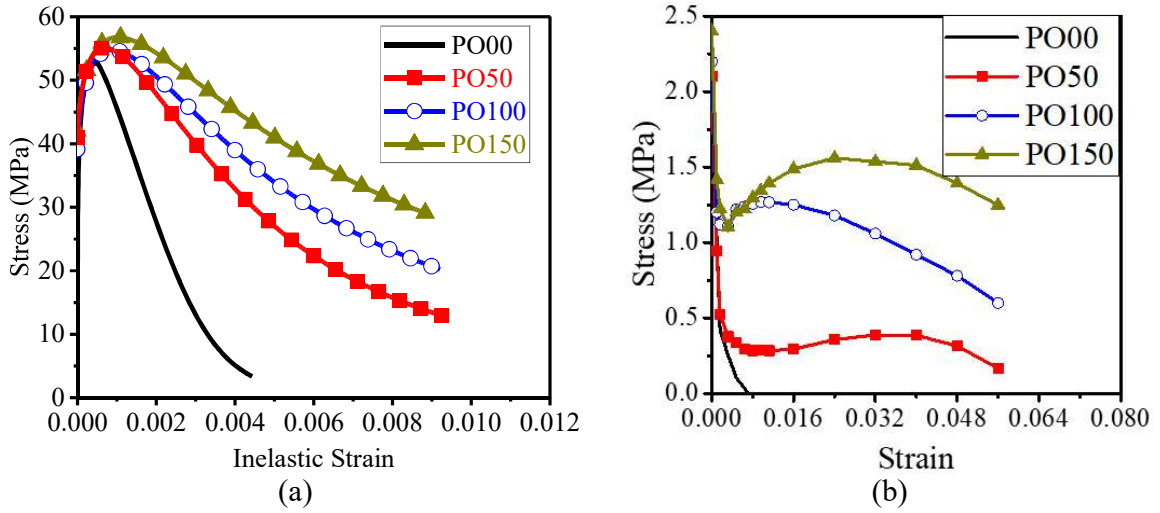


Figure 11. MSF concrete stress-strain properties: (a) Compression, (b) Tension

The damage in compression (d_c) and damage tension (d_t) is calculated as per **Equation (1)** - **Equation (2)** based on Huang and Liew [48]. The damage variables are a function of stress, elastic modulus, and strain in concrete.

$$d_c = 1 - \frac{\sigma_c + n_c f_{ck}}{E_c (n_c \sigma_c / E_c + \varepsilon_c)} \quad (1)$$

$$d_t = 1 - \frac{\sigma_t + n_t f_t}{E_c (n_t \sigma_t / E_c + \varepsilon_t)} \quad (2)$$

Where σ_c is stress, and f_{ck} is the compressive strength of concrete, E_c is the elastic modulus of concrete, n_c and n_t are the constant factors for compression and tension respectively, ε_c is the concrete strain in compression, and ε_t is concrete strain in tension which should be larger than zero.

The notched beams reinforced with macro synthetic fibre were tested. The fracture energy (G_f) is calculated as per JCI-S-001-2003[49]. The tensile strength from the inverse analysis [42] is used as tensile behaviour as input for concrete. The multi-linear stress-strain response obtained from inverse analysis (**Figure 11**) is used as input for inelastic strain and damage (d_t) parameters.

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5.2 Concrete Damage Plasticity Model (CDPM)

The concrete damage plasticity model (CDPM) is widely used to represent the complex behaviour of quasi-brittle material like concrete. This model is used for modelling concrete under both monotonic and cyclic loading [27]. A three-dimensional eight-node element (C3D8R) in ABAQUS is used for modelling concrete. The stress-strain response of concrete includes elastic and plastic properties. The total strain of concrete is the combination of both elastic and plastic strains. The nonlinear portion of the stress-strain response of concrete represents the plasticity and damage response. Hence, it is essential to define the damage corresponding to the plastic strain of concrete. The damage variables in concrete represented as d_c and d_t compression and tension damage, respectively. The damage is identified in the range of 0 to 1. Here, 0 represents no-damage, and 1 represents full damage [7,26,50–52]. The yield criteria define the critical stress state beyond which plastic deformation initiates and leads to failure. Many researchers have developed a yield criterion based on strength under compression and tension [27,28]. A similar approach is adopted as CDPM in ABAQUS. Few researchers performed the test on concrete in different conditions such as uniaxial tension, biaxial tension, uniaxial compression and biaxial compression and developed failure envelopes [26,51]. For brevity, details on CDPM are not provided here and can be found elsewhere (ABAQUS [53]).

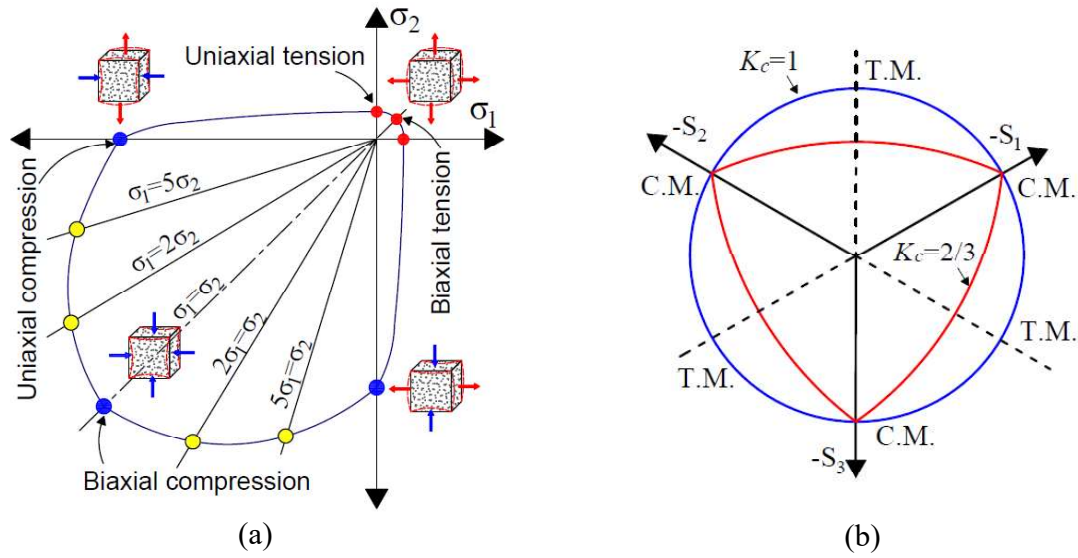


Figure 12. Yield criteria of concrete: (a) Concrete strength under biaxial stress, (b) Deviatoric cross-sections of the failure surface

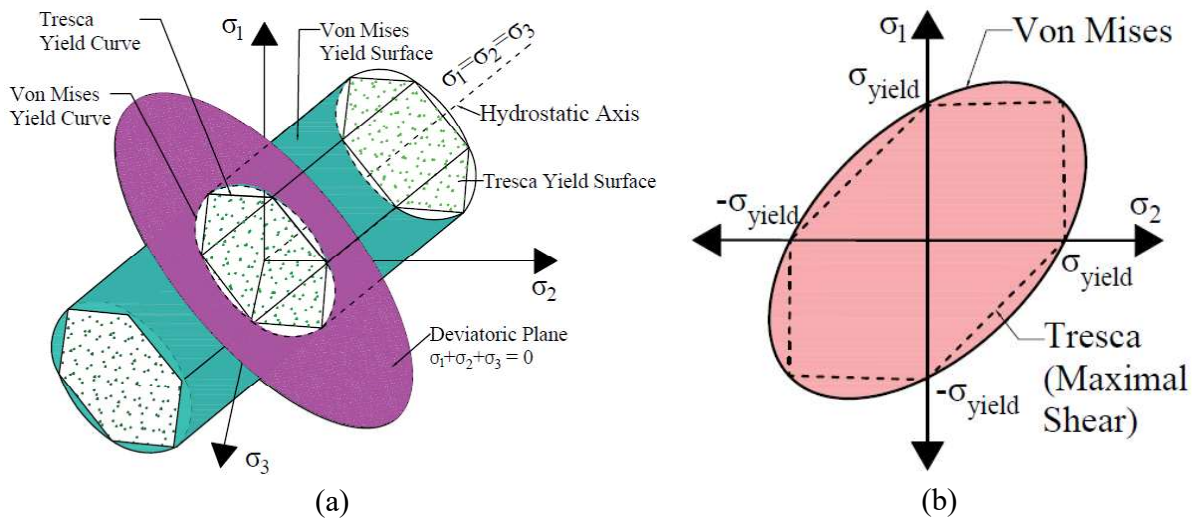


Figure 13. The different failure criterion for different stress models: (a) 3D schematic view, (b) Yield surface in 2D

The plasticity constants of concrete include dilation angle, eccentricity, stress ratio, shape factor, and viscosity parameter are shown in **Table 7**. The schematic view of yield criteria concrete and failure criteria are shown in **Figure 12** and **Figure 13**. Previous research shows that the dilation angle plays an important role in predicting peak load, post cracking behaviour, and failure mode

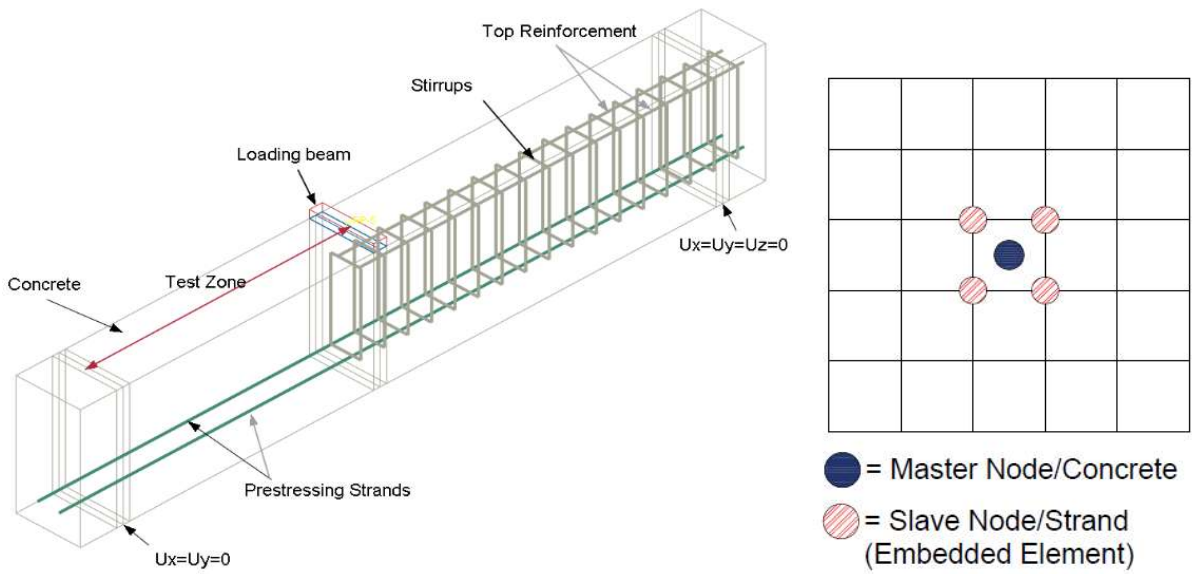
of beams [54–59]. From the sensitivity analysis, the dilation angle is chosen as 52.3° to simulate the experimental results closely. Other plasticity parameter values such as eccentricity, stress ratio, and shape factors are selected, such as default values. The analysis was carried out using ABAQUS/Standard, and the viscosity parameter term is activated [56]. The viscosity parameter is taken as 0.0005 for better convergence of the solution.

Table 7. Plasticity constants of concrete

Dilation angle (φ)	Eccentricity (ϵ)	F_{bo}/F_{co}	K_c	Viscosity Parameter (μ)
53.2°	0.1	1.16	0.667	0.0005

5.3 Prestressing Strands and Stirrups

The prestressing strand of length 1600 mm and with a cross-section of 98.4 mm^2 is modelled as a linear truss element (T3D2). The stress-strain properties of the strand were measured by a direct tension test, as shown in **Figure 6**, as explained in the experimental program. The same properties were converted as true stress-strain curve and implemented in FEM simulation. The pre-tensioning can be simulated by various modelling techniques such as initial stressing (default method). An initial prestress of 782.9 MPa is applied in each strand. The steel reinforcement of diameter 8 mm is used as secondary reinforcement. These secondary reinforcements were assigned with linear truss element (T3D2). The location of the stirrups and top reinforcement details are shown in **Figure 14 (a)**. Steel reinforcement is assumed to have elastic modulus ($E_{st} = 2 \times 10^5 \text{ MPa}$) and Poisson's ratio of 0.3. Both the high-strength prestressing strand and rebars were embedded in concrete. The embedment technique enables one or more elements to be embedded inside the host element. This technique does not require the modelling of the contact surface, and it eliminates the calculations of surface formulations [60]. The rebar node is defined as a master node, and



(a) (b)
Figure 14. FE Modelling (a) Schematic view of prestressed concrete beam elements, (b) Strand slave nodes and concrete master nodes

5.4 Loading and Boundary Conditions

Loads were applied in two stages. The prestressing load was applied in the first stage, followed by the external load in a displacement control mode. Simple support boundary conditions are imposed in FEM modelling, as shown in **Figure 14 (a)**.

5.5 Load-Deflection Behaviour and Failure Modes

FE models of fibre-reinforced prestressed concrete beams with different dosages were developed and analysed. The load-deflection behaviour and failure modes are shown in **Figure 15** and **Figure 16**, respectively. The load-deflection response of control (MSF00) and fibre reinforced concrete

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392 beam (MSF50 and MSF100) is predicted well up to the ultimate load. In the case of MSF150 beam,
393 the load-deflection behaviour is little offset to that of observed behaviour. The failure mode of all
394 the prestressed concrete beams was in direct shear tension. The comparison between experimental
395 and FE simulation responses are shown in **Figure 16**.

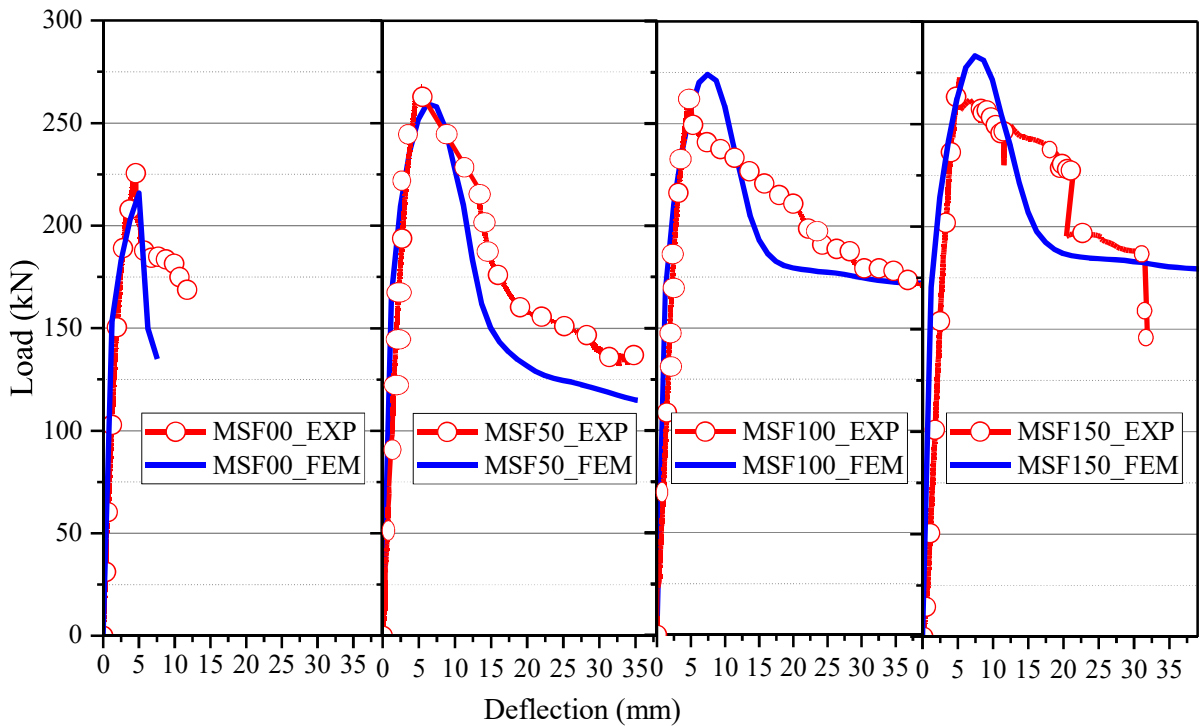


Figure 15. Load-deflection response of MSFRPC beams subjected to shear dominated loads

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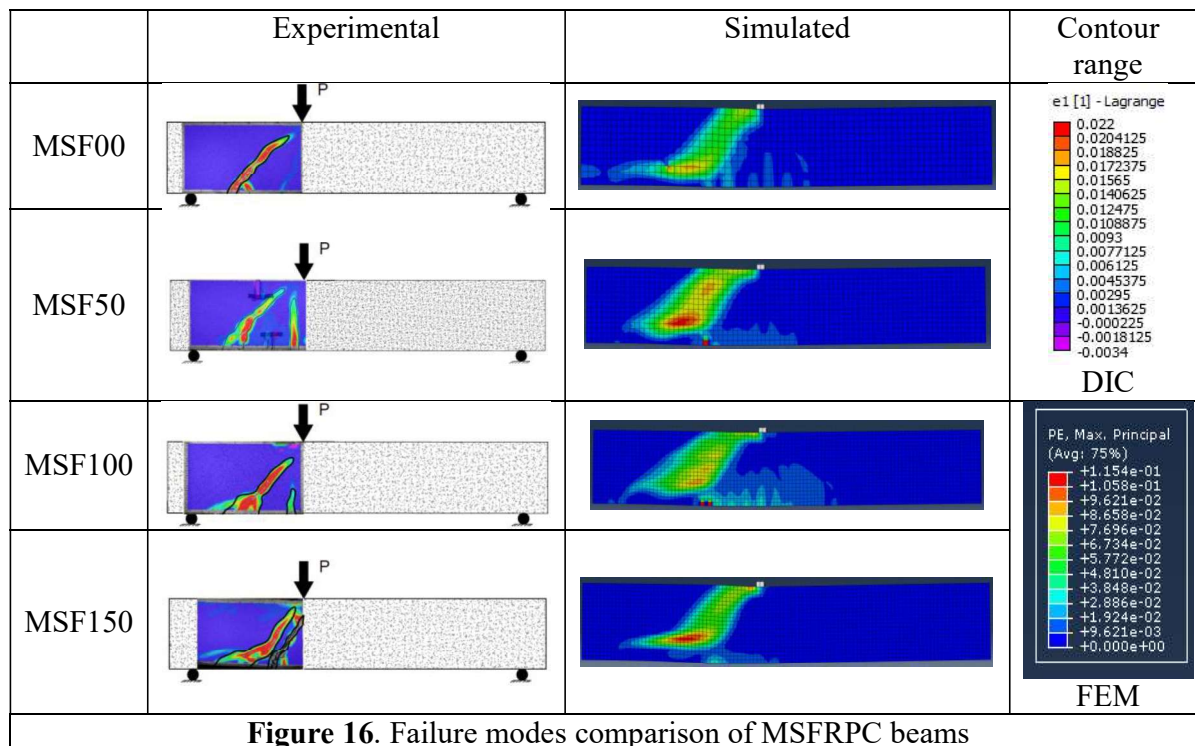


Figure 16. Failure modes comparison of MSFRPC beams

5.6 Parametric Studies

The shear capacity of prestressed fibre reinforced concrete beams depends on the concrete compressive strength, level of prestressing, shear reinforcement ratio, and fibre volume fraction. Experimental validation of 0.0%, 0.5%, 1.0% and 1.5% volume fraction were studied. In this parametric study, the influence of the prestressing level is focused on the different volume fractions of fibres at the same shear span to depth ratio of 2.4. With the increase in the level of prestressing, the shear capacity of the beams increased, as shown in Figure 17.

The increase in the prestress level does not increase the shear strength significantly for the control beam (MSF00). For a higher prestress level of $0.8 P_u$, the specimen failed in a premature shear compression mode. In fibre-reinforced beams, a limited increase in shear strength (between 9% to 11%) was observed due to an increase in prestress levels. Figure 17 shows that there is not much

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412 improvement in shear capacity after 60% of increment in prestressing. The MSFRPC beams of
 413 different levels of prestressing, such as 60%, 70%, and 80% failed in shear mode, as shown in
 414 **Figure 18**. The shear strength is enhancement is due to prestressing, which delayed the formation
 415 of shear cracks and helped in controlling the crack opening.

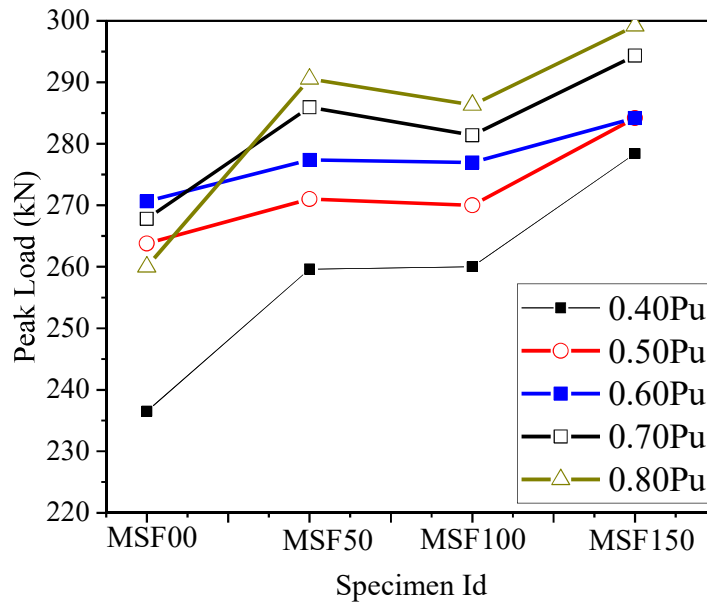


Figure 17. Parametric study on the level of prestressing

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Beam ID	0.6P _u	0.7P _u	0.8P _u
MSF00			
MSF50			
MSF100			
MSF150			

Figure 18. Failure modes of MSFRPC beams at different level of prestressing

6.0 SHEAR CAPACITY PREDICTIONS BY RILEM AND FIB-MC2010 PROVISIONS

The shear capacity of MSFRPC beam is calculated by using RILEM [43] and Fib- MC2010 [61] code provisions. The average tensile strength of FRC as per RILEM provisions is used for estimating the shear capacity of beams.

6.1 Shear capacity calculations using RILEM recommendations (V_{RILEM})

The shear capacities (V_{RILEM}) formulations in RILEM recommendations [43] include three components such as shear resistance of member without shear reinforcement (V_{cd}), shear resistance due to discrete fibres (V_{fd}) and shear reinforcement/stirrup contribution (V_{wd}). The shear resistance of member without shear reinforcement (V_{cd}) includes the resistance due to un-cracked concrete, aggregate interlock, dowel action, and initial prestress. Similarly, shear resistance due to fibres (V_{fd}) includes factor accounting for the flange of T-sections and depth factor. The flange contribution is taken as one for rectangular beams. Other parameters were calculated as per the sectional details of the test specimens. The resistance offered by fibres in tension at a CMOD of 3.5 mm is used for shear contribution of fibres. These residual flexural tensile strengths vary based on fibre dosage and type of fibres and strength of concrete. The shear capacity of the tested MSFRPC beams using the RILEM equations are shown in **Figure 19**. Comparison of test results and predictions shows that the shear capacities of all the test specimens were conservatively estimated.

6.2 Shear Predictions using Fib-Model Code2010 Provisions (fib-MC2010)

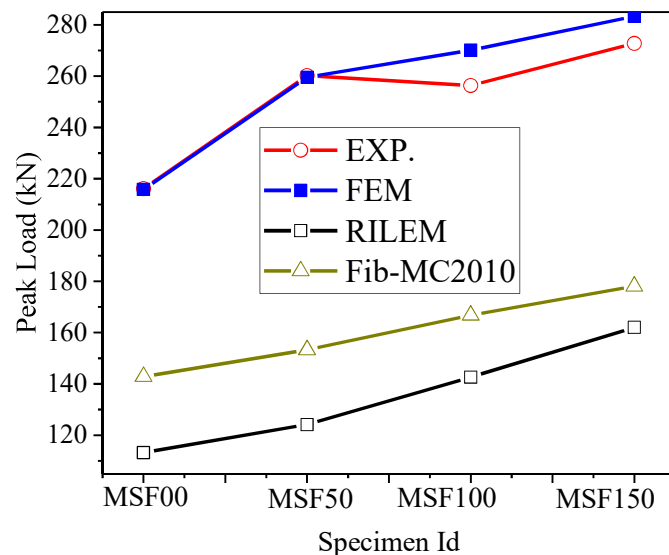
Fib-MC2010 code [61] explicitly includes several parameters in the shear capacity calculations ($V_{Rd,F}$). The parameters included in Fib-MC2010 for shear estimations include: (i) reinforcement

ratio of longitudinal bars (ρ_l), (ii) size effect factor which accounts the size influence on shear capacity of beam (K), (iii) concrete compressive strength (f_{ck}), (iv) average prestressing stress acting on the cross-section of concrete due to prestressing action (σ_{cp}), (v) fracture parameters such as ultimate residual tensile strength (f_{Ftuk}) and characteristic value of tensile strength of concrete matrix (f_{ctk}). The residual tensile strength of FRC was calculated at the CMODs of 0.5 mm and 2.5 mm. Based on the experimentally observed fracture test results (f_{R1} and f_{R3}), the residual tensile capacities (f_{Ftuk}) of different fibre dosages were calculated using the equations shown in **Table 8**. In these calculations, the partial safety factor of the concrete material is considered as 1. The obtained shear capacity of MSFRPC beams is shown in **Figure 19**.

Table 8. Shear capacity equations of RILEM recommendations and Fib-MC2010 provisions

Code	Capacity (V)	Theoretical Shear Capacity Formulas
RILEM	Concrete (V_{cd})	$V_{cd} = \left[0.12 k (100 \rho_l f_{ck})^{\frac{1}{3}} + 0.15 \sigma_{cp} \right] b d$, $k_l = k = 1 + \sqrt{\frac{200}{d}} \leq 2$ $k_f = 1 + n \left(\frac{h_f}{b_w} \right) \left(\frac{h_f}{d} \right) \leq 1.5$, $n = \left(\frac{b_f - b_w}{h_f} \right) \leq 3$, $\rho_l = \frac{A_s}{bd} \leq 0.002$
	Fibres (V_{fd})	$V_{fd} = 0.7 k_f k_l \tau_{fd} b d$, $\tau_{fd} = 0.12 f_{RK,4}$
	Prestress (σ_{cp})	$\sigma_{cp} = \left(\frac{N_{sd}}{A_c} \right)$
Fib-MC2010	Concrete ($V_{Rd,F}$)	$V_{Rd,F} = \left\{ 0.18 K \left[100 \rho_l \left(1 + 7.5 \frac{f_{Ftuk}}{f_{ctk}} \right) f_{ck} \right] + 0.15 \sigma_{cp} \right\}^{1/3} b_w d$ $f_{Ftu}(w_u) = f_{Fts} - \frac{w_u}{2.5} (f_{Fts} - 0.5 f_{R3} + 0.2 f_{R1}) \geq 0$ $f_{Fts} = 0.45 f_{R1}$, $f_{ck} = f_{cm} - 8$, $f_{ctm} = 0.3 f_{ck}^{2/3}$
	Prestress (σ_{cp})	$\sigma_{cp} = \left(\frac{N_{sd}}{A_c} \right)$

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 4 454 The ratio of experimental to theoretically calculated shear capacity of MSFRPC beams is 1.5, 1.7,
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 7 455 1.5, and 1.5 for MSF00, MSF50, MSF100, and MSF150, respectively. The prediction comparison
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 9 456 of fib-MC2010, RILEM, and FEM predictions show that the FEM results closely predict the test
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 11 457 results than the existing code provisions (**Figure 19**). Not many studies have focused on the
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 14 458 performance improvement of prestressed concrete beams under shear through macro synthetic
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 16 459 fibre addition. More experimental research on macro-synthetic fibre reinforced concrete beams
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 19 460 under shear loads for a wide range of parameters is required to develop a rational shear capacity
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 21 461 model for design purposes. It is a scope for future work.
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 45 **Figure 19.** Comparison of shear capacity predictions with experimental and FEM predictions
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48 464 7.0 SUMMARY AND CONCLUSIONS

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 51 465 The shear behaviour of MSFRPC concrete beams was studied through experimental and numerical
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 54 466 means. The effect of volume fraction of macro synthetic fibres was considered. Tension stress-
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 56 467 strain response of macro synthetic FRC obtained from the inverse analysis was used as input for
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 59 468 FEM analysis. The nonlinear three-dimensional finite element models were developed, and the
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4 469 predictions were validated with test results. The load-deflection response and failure modes were
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7 470 compared with FEM results. After that, a detailed parametric study was performed by varying the
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9 471 level of prestressing. Based on this limited study, the following conclusions can be drawn:

- 11 472 1. The fracture test results revealed that the macro synthetic fibres are effective at higher crack
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13 473 opening displacements higher than 2.5mm. Due to addition of macro synthetic fibers of 1.0%
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15 474 and 1.5% of volume fractions, the fracture energy increased by 9.6 and 16 times compared to
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21 476 2. The failure mode of prestressed concrete beams changed from brittle to ductile mode due to
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24 477 the addition of fibres at 0.5%, 1%, and 1.5%. The energy absorption capacity increased by
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26 478 3.7, 4 and 6 times for 0.5%, 1.0% and 1.5% volume of fibre addition.
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29 479 3. The predictions of load-deflection and failure mode using the finite element approach adopted
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31 480 in this study closely matched the test results. Parametric studies showed that the shear capacity
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33 481 of prestressed concrete beams increased by up to 18 % with an increase in fibre dosage and
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36 482 up to 15% due to increase in level of prestressing.
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39 483 4. The shear capacity estimations by RILEM and fib-MC2010 code predictions are very
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41 484 conservative compared to FE predictions. More research is required on macro-synthetic fiber
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43 485 reinforced concrete beams to improve the existing code provisions.
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491 sponsoring the materials required for this research. Specimens were cast at the precast yard of
492 PRECA India Pvt. Ltd.

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494 **9.0 CONFLICTS OF INTEREST**

495 None.

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497 **10.0 DATA AVAILABILITY STATEMENT**

498 Some or all data and models that support the findings of this study are available from the
499 corresponding author upon reasonable request.

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